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Using Activated Carbon/Clay-Based Thin Layer Capping for Mercury-Contaminated Sediment Remediation: Microcosms Study

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本論文係 丁昱 君(學號 R05541212)在國立臺灣大學環境工 程學研究所完成之碩士學位論文,於民國 108 年 7 月 5 日承下列 考試委員審查通過及口試及格,特此證明

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中文摘要

近年來,現地薄層覆蓋法技術之突破為整治汞汙染底泥帶來新的可能性,也提 供除疏濬法以外新的整治策略。本研究分為兩部分,利用數種活性碳/黏土基之薄 層覆蓋層在微型系統中評估整治汞底泥之可能性。在本研究第一部分中,自製之含 硫活性碳(SAC)在等溫吸附實驗中發現對於二價汞及甲基汞之吸附親和性(KD 值分 別為 9.42×10⁴ 及 7.66×10⁵)比起其原始活性碳(AC)有顯著提升(KD 值分別為 3.69×10⁴ 及 2.25×10⁵)。但在底泥競爭吸附實驗中, AC 對比 SAC 對於汞底泥(14.2-235.8 mg-Hg/kg)中具有較佳之汞溶出抑制能力,並在3%添加量下具有最佳之汞溶 出抑制效率(99.88%)。其原理可能為 SAC 在吸附實驗平衡後形成穩定的 HgS (s)奈 米顆粒,使底泥競爭吸附實驗之 AC 抑制汞溶出之能力優於 SAC。另外,研究之 各式覆蓋層(SAC+皂白土、SAC+低汞底泥、AC+皂白土)在上流式微型系統中對於 總汞及甲基汞均具有良好溶出抑制能力。在本研究第二部分為探討底泥擾動事件 對於覆蓋穩定之影響,開發一具有自製震盪系統之橫向流微型系統。三種不同黏土 材料之活性碳/黏土基覆蓋層施加於實場汞底泥中(76.0±2.59 mg-Hg/kg),發現 AC(3%)+皂白土(3%)以及 AC(3%)+高嶺土(3%)在模擬橫向流及表層底泥擾動之條 件下,對於實場底泥中總汞及甲基汞皆能達到約75-95%及64-98%之溶出抑制效 果達75天之久(實驗全時程)。而AC(3%)+蒙脫土(3%)的薄層覆蓋層由於蒙脫土在 水中沉降性及穩定性較差,使總汞及甲基汞溶出抑制效率不佳。本研究發現穩定性 高之薄層覆蓋層有較佳之汞溶出抑制能力,並於間歇性底泥擾動下有較佳之抵抗 能力;而穩定性較差之薄層覆蓋層可能造成甲基汞大量溶出。

關鍵字: 汞、甲基汞、底泥整治、薄層覆蓋法

II

Abstract

The breakthrough of in-situ thin layer capping technology in recent years has shed light on the remediation of Hg-contaminated sediment and provides a promising alternative besides traditional dredging. In this thesis, the plausibility of several activated carbon (AC)/clay-based thin layer caps were demonstrated in two microcosm studies. In the first study, a lab-synthesized sulfurized activated carbon (SAC) performed greater sorption affinity to both aqueous Hg^{2+} (K_D=9.42×10⁴) and MeHg (K_D=7.66×10⁵) compared to those for raw activated carbon ($K_D=3.69\times10^4$ and 2.25×10^5 , respectively) in isotherm adsorption tests. However, AC appeared to have greater sequestration ability than SAC in Hg-spiked sediment (14.2–235.8 mg-Hg/kg), with the optimistic dosage of 3wt% AC causing reduction of THg with 99.88%. It may suggests that possibly formed nano-HgS particles could be released thus elevates the porewater Hg when SAC existed. Also, a 83-d trail of up-flow microcosms was demonstrated with various caps (SAC + bentonite, SAC + clean sediment, and AC + bentonite) and all observed significant inhibition of both THg and MeHg. In the second study, a horizontal-flow microcosm with lab-made vibration system was designed to evaluate the capping efficiency during turbation events. AC/clay-based caps with clay combinations were applied to actual Hgcontaminated estuary sediment (76.0±2.59 mg-Hg/kg). The caps with AC + bentonite and AC + kaolin were efficient in reducing both total mercury (THg) and methylmercury (MeHg) concentrations in overlying water by 75–95% and 64–98%, respectively in the later stage of 75-d operation. In contrast, the AC (3%) + montmorillonite (3%) cap did not show a significant reduction on THg and MeHg in overlying water, probably due to the unstable, suspension property of montmorillonite. The stable caps showed higher resistance to Hg breakthrough under occasional turbation events; however, a labile cap

appeared to have dramatic Hg breakthrough when turbation occurred. It is therefore essential to note that with unstable caps, turbation events may result in unwanted secondary resuspension of contaminants.

Keywords: mercury, methylmercury, sediment remediation, thin layer capping

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Chapter 1 Introduction

Mercury (Hg) has been recognized as one of the most toxic heavy metal due to its high volatility, persistence, and bioaccumulation to human beings or natural biota [1]. Hg, in general, exists in the form of divalent Hg (i.e., Hg²⁺) in the aqueous phase and may transforms to methylmercury (MeHg), which is one of the most toxic Hg forms via biomethylation under an anoxic sediment environment [2]. Although ex-situ strategies have been proven promising in removing Hg out of sediment [3, 4], problems such as unfeasible cost [5], resuspension of contaminants [6, 7], and production of contaminated sediment residues [6, 7] may discourage their application. Therefore, the development of novel and feasible techniques in remediating Hg-contaminated sediment is highly needed.

The breakthrough of using in-situ thin layer capping, or "in-situ active capping," to remediate contaminated sediment has drawn much attention in the past decade. In particular, using activated carbon-based thin layer capping to sequestrate persistent organic pollutants (POPs) has received promising effects on some full-scale sites [8-11]. This breakthrough also shed light on the remediation of Hg-contaminated sediment, which is the other major polluted sediment within concern.

There are several knowledge gaps that have to be filled up before thin layer capping be put to application. One of which is the development of sorption materials with better stability and Hg sorption affinity. Sulfur-impregnated activated carbon (SAC) has been verified to enhance Hg adsorption capacity than its raw AC precursor in aqueous adsorption tests [12-14]. However, studies on using SAC as the thin layer capping material for inhibiting the release of Hg and MeHg from sediment environment are scarce.

One of the other major knowledge gaps for the thin layer capping is its capping

stability and the potential risks of Hg escape from caps. The sediment turbations caused by bioturbation or physical erosion have been identified as critical mechanisms in contaminant transport in the natural aquatic environment [15-18]. It is intriguing how sediment turbation may affect the efficiency of the thin layer capping in treating Hgcontaminated sediment, but related studies remain with little information.

In this master thesis, the plausibility of thin layer caps to remediate Hg-contaminated sediment was discussed and the activated carbon/clay-based thin layer caps were demonstrated in two microcosm studies. In chapter 2, a brief review is provided for practical details about Hg management and thin layer capping in real site application. The first study (chapter 3) addressed the Hg sorption behavior of a lab-made coconut-based SAC to mercury-containing sediment remediation by thin layer capping method via batch and microcosm experiments. The second study (chapter 4) evaluated the Hg leaching inhibition performance of thin layer caps under horizontal flows and artificial sediment turbation operated in microcosms.

Chapter 2 Hg Management and Thin Layer Capping

2.1 Mercury Risk and Global Management Efforts

Mercury (Hg) has been recognized as one of the most hazardous heavy metals due to its high volatility, persistence, and bioaccumulation in human beings and natural biota [1]. Long-term, high-dosage exposure of humans to Hg may pose risk to the brain, heart, kidneys, lungs, and the immune system by causing various neurodegenerative diseases, such as Minamata disease, Alzheimer's disease, and Parkinson's disease [1, 19-22]. Hg can be released from both natural or anthropogenic sources. With elevating human industrial activities, much Hg has been mined out of the earth and discharged to the environment as waste. Major anthropogenic Hg sources include gold mining, coal combustion, and metal production [1, 3, 23-25], which have created a huge amount of Hg-containing wastewater to be discharged into wetlands, rivers, and seawater. Amos et al. [26] estimated that around 5500 \pm 2700 Mg of aquatic Hg is released into rivers annually across the globe. Excluding natural mobilization of Hg from terrestrial ecosystems, Kocman et al. [27] estimated riverine discharge of Hg with a smaller value of around 800 to 2200 Mg/year.

Global efforts on Hg management have been put together through the Minamata Convention on Mercury, a global treaty to protect human health and the environment from adverse effects of Hg. Updated on August 2018, 128 nations have signed the treaty with requirements including banning of primary Hg mining, reductions in Hg release to the environment (air or water), exposure through products and consumptions, remediation of contaminated regions, monitoring, outreach, and other means.

As Hg is discharged into the aquatic environment (i.e., wetlands, lakes, and coasts),

sediments may serve as the sink for Hg [28], which is mainly in the form of mobile divalent mercury (Hg²⁺) and may transforms to monomethyl mercury (MeHg) and gaseous mercury (Hg⁰) through resuspension and diffusion [29, 30]. Sediment suspension can be induced by natural physical processes (e.g., waves and storms) [31, 32], anthropogenic activities (e.g., dredging, trawling, and boating) [33] and biological activities (e.g., bioturbation) [34].

Hg in natural waters occurs in forms including Hg⁰, ionic mercury (e.g., Hg⁺ and Hg²⁺), and methylated mercury (e.g., CH₃Hg⁺, (CH₃)₂Hg) [35]. While all forms of Hg are toxic, its methylated form, MeHg, is specifically problematic. MeHg has high bioaccumulation and biomagnified ability and poses a threat to biota and human [36]. MeHg usually occurs in minor proportions, at around 0.1–1.5% of total Hg [37-40] in anoxic sediment environments, but can pose a high risk to human health.

Much effort on Hg control has been put in water treatment and sediment remediation. For wastewater treatment of Hg, lime softening, chemical precipitation, coagulation, reverse osmosis, ion exchange, and membrane filtration have been considered [41]. As for sediment and groundwater Hg remediation, many techniques have been employed, such as adsorption, biosorption, ion exchange, chemical precipitation, reduction, and stabilization/fixation. Among these methods, adsorption and stabilization/fixation have been proved to be the most practical techniques [24, 42, 43]. Dredging followed by exsitu methods have been commonly executed due to its long-term effectiveness and relatively short remediation period [5]. However, dredging can be preventatively costly. Also, dredging may cause remobilization of contaminants during remediation, and may inevitably retain contaminants, posing a long-term threat [44].

4

2.2 In-situ Approach and Thin Layer Capping

One of the main advantages of in-situ technologies is that they used toward reducing environmental impacts and avoiding the huge cost of dredging. The main challenges are related to the difficulties in ensuring that the contaminants are effectively reduced by the technologies due to the heterogeneity of sediment and the uncertainty in the distribution of contaminants. In-situ technologies require a treatability test to evaluate their efficiency at the specific site [45].

A relatively new term of "thin layer capping", which involves the use of chemically reactive materials to sequestrate contaminants to reduce their mobility, toxicity, and bioavailability in sediment. The remediation cost of thin layer capping is likely to be smaller than for conventional strategies (e.g., dredging or sand capping). Additionally, thin layer capping may further enhance or improve habitat recolonization by benthic organisms [46]. Active materials, such as activated carbon, have been shown to reduce the toxicity of persistent organic pollutants (POPs) such as polychlorinated biphenyls (PCBs), polycyclic aromatic hydrocarbons (PAHs), or pesticides in laboratory or field studies [47-56]. Updated in 2015, more than 25 field studies have been conducted by thin layer capping approaches [57] (Table 2-1).

5

Table 2-1. Field application cases for thin layer capping remediation. (Partially

adopted from Patmont et al.[57])

| location | pollutants | Engineering method | Remediation performance | Ref |
|---|------------------|--|--|------|
| Hunters Point Shipyard, USA | PCBs | Mixed –3.7% of AC into 1 ft. deep of sediment. | Bioaccumulation of clam decrease 62% after capping for 7 months. | [58] |
| South Basin, USA | PCBs | Mixed 2.0~3.2% of AC into 30–40 cm deep of sediment. | Surface water PCBs conc. decrease 90% after capping for 18 months. | [8] |
| Hunters Point Shipyard, USA | PCBs | Mixed –3.7% of AC into 1 ft deep of sediment. | PCBs conc. reduce 73% in passive sampler. | [59] |
| Trondheim Harbor, Norway | PAHs, PCBs | Pre-mixing of AC, clay and sand into slurry, followed by direct capped on the surface of sediment. | AC-clay mixing caps have highest in conc. decrease during 9–12 months sampling, no obvious impact on biodiversity. | [9] |
| Eidangerfjord and Ormerfjord, Norway | PCBs, furans | Pre-mixing of AC(2%) and clay, followed by direct capped on the surface of sediment. | During 20 months capping, conc. of low- chloride PCBs decrease >90%, while high- chloride PCBs decrease 60–70% in porewater. | [60] |
| Eidangerfjord and Ormerfjord, Norway | PCBs, furans | Pre-mixing of AC(2%) and clay, followed by direct capped on the surface of sediment. | After 2 yrs of capping, control site decrease pollutant flux 70–90%, while capping sites decrease 50–60%. After 3–5 yrs, capping sites decrease 80–90%, while control sites reduce 20–60%. | [61] |
| St. Lawrence River, USA PCBs | | Spraying, mixing, and injecting of mixture containing two AC on to sediment | PCB bioaccumulation of benthic organisms decrease 69–93% during 3 yrs of capping. Porewater conc. decrease 93%. | [10] |
| Lower Canal Creek, USA | PCBs, DDT, Hg | Direct spraying of AC(SediMite®) | During 10 months of capping, PCBs and DDT bioaccumulation have dramatic decrease, MeHg decrease for 50%. | [62] |
| Grenland fjords, Dioxins, lim Norway Hg dire | | Pre-mixing of AC, clay and limestone into slurry, followed by direct capped on the surface of sediment. | Up to 90% biodiversity reduction have been observed in AC capped sites, capping using non-AC material have smaller bio-impact. | [63] |

2.3 Capping Materials

For the application of thin layer capping on Hg-contaminated sites, laboratory studies have been conducted using AC [14, 57, 64-66], biochar [64, 67], or surface-modified black carbon [14] to immobilize Hg. Some studies have shown that the amendment of black carbon may successfully reduce bioavailable Hg and MeHg to benthic organisms [65, 66]. Beside bench-scale studies, several field-scale studies [62, 68] have also been carried out to and observed with moderate success in reducing Hg in porewater or biotas.

Activated carbon (AC) is composed of defective graphene layers, which are formed by gasification of carbon atoms via activation (often by thermal treatment). After activation, AC can be filled with pores that greatly increase surface area (as high as 500– 1500 m²/g; [24]) and intensify van der Waals force. With its high specific surface area, AC has proven to be a promising option for remediation of contaminated sites for not only organic pollutants[47-56] but also Hg [64-66, 68, 69]. AC has several kinds of acid functional groups such as carboxyl groups on its surface, and are expected to chemically adsorb Hg [13].

Nevertheless, the sorption capacity of AC toward Hg is still limited due to the nonpolar characteristics of activated carbon, which hinder interactions between charged metal species and the solid surface [43].

The other main concern of applying black carbon to sediment remediation is its possible adverse effects on the benthic organisms itself. One-fifth of previous studies have reported adverse bio-effects using black carbon to sequestrate Hg [70]. Benthic biotas suffered from reduced species richness, biomass loss, reduced feeding rate, organ damage, or reduced growth after carbon amendment. Several studies suggested that the

possible explanations are because the black carbon may reduce nutrients' bioavailability [71], or reduce ingestion rate by harming gut structures [72].

SAC has been verified to enhance Hg adsorption capacity than its raw AC precursor in aqueous adsorption tests (Table 2-2; [12, 13, 41, 73, 74]. Sulfurization of AC enhance Hg sorption capacity in most essays [12, 13, 41, 73, 74] and sometimes over 100% by magnitude [12, 13]. For example, Wang et al. [12] demonstrated that an increase in Hg adsorption capacity of coconut AC from 150 to 820 mg/g by sulfurization with sulfur powder (C/S ratio: 1:2) was shown. Li et al. [13] increased Hg adsorption capacity of coke from 315.8 to 694.9 mg/g by impregnated the coke with sulfuric acid (80°C, 13 h). Also, the stability of Hg sorption to SAC was also known to increase as Hg was found stably sorbed to SAC in a broad pH range [12]. However, SAC has yet been tested to apply on Hg-contaminated sediment.

Biochar is another attractive sorbents as a potential remediation material since it is less costly than AC and may play the role of fertilizer if applied in soil [75]. Similar to AC, biochar is a porous, carbon-rich, black carbon material produced by thermally decomposing biomass under low-oxygen concentrations and temperatures between 300– 1000°C. Gomez-Eyles et al. [64] conducted an experiment testing Hg sorption affinity of 13 kinds of biochars and 4 kinds of AC, the results showed that both AC and biochar have efficient Hg sorption affinity with AC superior in Hg²⁺ sorption.

Clay is a general term for a broad range of inorganic mineral with the size within 2 mm. With good thermal stability, cation exchange capacity, and settling clay may be the other potential capping material [76]. Clay minerals could be further modified to organoclays, and was reported to enhance sorption capacity up to 10–30 times to Cr, As,

Pb, Cd, and Zn [77-79].



| Raw materials | Activation method | S _{BET} (m /g) | S (%) | | on conditions emperature/pH) | | Hg Sorption capacity (mg/g) | Reference |
|------------------|---|----------------------------|-------|-------------------------------|---------------------------------|-------------|--------------------------------------|-----------|
| Sugar cane | SO_2 and H_2S 400°C, 30 min | 500.05 | 8.9 | | 30°C | 6 | 188.68 | [73] |
| | Non-sulfurized | 1884 | 0 | | 25°C | 5.5 | 150 | |
| Coconut | Sulfur powder, S:C=1:2 400°C, 2 h | -1000 | 22 | | | | 820 | [12] |
| | Non-sulfurized | 193.7 | 1.39 | | 25°C | 5 | 315.8 | [13] |
| Coke | H ₂ SO ₄ , 80°C, 13 h | 136.7 | 3.33 | | | | 694.9 | |
| Almond seed | Activated by phosphoric acid $+C_2S$ sulfurization, S:C=2:1 600°C, 1 h | 1637 | 9.9 | HgCl ₂ solution | 25°C 35°C 45°C 25°C | 6 3 8 | -230 -280 -290 -190 -230 | [41] |
| | Non-sulfurized | 828 | 1.5 | | 30°C | 7 | 455 | [74] |
| Coal | Dimethyl disulfide 30°C, 48 h | 348 | 9.6 | | | | 441 | |
| | Sulfur powder, S/C=4:1 145°C, 30 min 600°C, 30 min | 596 | 10.8 | | | | 529 | |

Table 2-2. SAC enhances Hg sorption capacity in aqueous adsorption tests.

Iron sulfide minerals (Fe_xS_y) have been found to have good immobilizing ability to double-valent metals, such as Mn^{2+} , Ca^{2+} , Mg^{2+} , Ni^{2+} , Cu^{2+} , Cd^{2+} , Co^{2+} , Zn^{2+} , Pb^{2+} , and Hg^{2+} [80-85], basically due to their adsorption or precipitation properties. In addition, iron sulfides have also been reported to degrade organic contaminants by reduction mechanisms. The common forms of iron sulfide minerals include mackinawite (FeS), greigite (Fe₃S₄), pyrite (FeS₂), and pyrrhotite (Fe_{1-x}S) [86]. In earlier research,

mackinawite, pyrite, and pyrrhotite have been shown to have high potential to sequestrate Hg [87, 88]. Some of the more recent studies have been conducted using lab-made nanomackinawite to sequestrate Hg. Liu et al. [86] reported FeS with adsorption capacity up to 1700 mg/g (by calculation) at pH = 5.6; more than 99% Hg was removed at Hg/FeS ratio < 1000, with 77% of the removal by precipitation and 23% by adsorption (Hg/FeS = 0.22). Sun et al. [89] found that commercial pyrite had lower Hg sorption capacity (9.9 mg/g) as compared to lab-synthesized mackinawite (769.2 mg/g), probably due to the smooth surface of pyrite. Skyllberg and Drott [90] conducted a slurry batches study, discovering that the dosage of 2% FeS in 5000 µg-Hg/g organic-rich soil may outcompete O/N ligands in sediment for Hg sorption, resulting in 50% Hg sorbed on FeS to form HgS4 (metacinnabar). As the ratio of FeS increased to up to 20%, a complete outcompete with 100% Hg sorbed on FeS was observed.

To date, a promising active material in remediating Hg-contaminated sites is yet to be proven with good adsorption efficiency, stability, and eco-friendliness. Consequently, further research is needed in several areas, including (1) fabricating novel capping materials with good adsorption affinity for Hg or other heavy metals; (2) establishing competitive adsorption models of amendments in sediment condition to evaluate real adsorption outcomes in nature disturbance; (3) introducing amendments with biological tests to prove the efficiency of reducing Hg bioavailability; (4) developing efficient, lowimpact capping delivery systems; (5) assessing long-term stability and ecological recovery of placing active caps; (6) conducting life-cycle analysis for thin layer capping remediation.

2.4 Real Site Practice

In real site application, thin layer capping can be performed in two existing methods:

(1) mechanical mixing amendment; (2) spray thin layer capping. Mechanical mixing amendment involves applying of capping materials and mixing of materials into top layer of sediment. Several advantages of mechanical mixing amendment can be anticipated, such as better transportation of materials, less material lost by water flow, or less possibility of adverse effect to benthic organisms [9, 58]. However, mechanical mixing amendment also tends to mobilize sediment during engineering procedure, and is likely to be costlier due to the mixing of sediment. Cho et al. [8] demonstrated two types of machinery to perform mechanical mixing amendment (Figure 2-1). The first machinery is modified by a rotary cultivator originally used for weeds removal in swamps. The second machinery, the injection system, was originally used for injection of cement to stabilize sediment.



Figure 2-1. Cho et al. [8] performed mechanical mixing amendment with (a) a rotary cultivator (Aquatic Environments, Inc.,) and (b) an injection system (Compass Environmental, Inc., GA).

Spray thin layer capping involves pre-mix of capping materials and directly spraying into the water body without further mixing. As the material sink to the bottom of the water body, a thin layer of cap formed on the surface of the sediment. With the assistant of benthic biotas, capping materials would be able to mix with the top of surface sediment, therefore immobilize pollutants in the porewater [9]. Menzie et al. [62] performed spray thin layer capping in a shallow wetland with a self-made spreader, consisted of a 250pound hopper and a diesel sprayer (Figure 2-2). Cornelissen et al. [60] performed a spray thin layer capping in a fjord with 100 m of water depth by using a spraying instrument in a ship (Figure 2-3). The ship was designed with 275 m³ water tank and a dredging pumps. The capping materials were premixed in the tank by a pump (500 hp), latter spraying through an elastic tubing in 10 m deep into the water by the other pump (204 hp). Spray thin layer capping appears to be more flexible in real site practice since it can be applied in both shallow or deep regions. Also, spray thin layer capping is less costly as it doesn't need additional mixing device. In addition, several studies [10, 51] have concluded that contaminants immobilizing efficiency did not differ with or without artificial mixing of sediment.



Figure 2-2. Menzie et al. [62] performed a spray thin layer capping using self-made equipment (Vortex TR Aquatic system).



Figure 2-3. Cornelissen et al.[60] premixed AC, clay and seawater and preformed a spray thin layer capping by a spraying system on a ship.

2.5 Estimation of Remediation Cost

Despite all technological difficulties, the cost of remediation may be just as important since sediment remediation can be quite costly and even to a degree of unrealistic. Remediation methods with "in-situ" strategies have huge advantages that they can be operated with reduced environmental impact and without costs associated with dredging [45].

As one of the most promising in-situ remedies, thin layer capping was studied of its remediation cost [5, 62]. The material cost and operational cost are two major portions of its cost. Some other portions of costs may also be needed on other aspects [62], including laboratory studies, construction of types of machinery, materials transportation etc. The cost of thin layer capping was estimated within the following paragraphs, with an exchange rate calculated by USD/NTD = 1:30, and Euro/NTD = 1:40.

Menzie et al. [62] compared several remedies (i.e. thin layer caps, sand caps, and dredging) with a case study in Canal Creek, Maryland. In the estimation, capping material

SediMite[®] costed US\$3,730 per ton (NTD\$111.9 per kg), slightly higher than commercial AC (NTD\$60–100 per kg); amendment dose was 4.53 kg/m²; instruments costed US\$23,000 (NTD\$690,000); deliver operation costed US\$14.085 per m² (NTD\$422.5 per m²); laboratory studies costed US\$23,500 (NTD\$700,000). As the results, to remediate 10 acres of sediment may cost US\$89,000 per acre (NTD\$6,640,000 per HA) by SediMite[®] thin layer caps. If applying dredging technology, the same 10-acre contaminated site may cost US\$800,000 per acre (NTD\$59,300,000 per HA) by dredging with 3 ft. Calculation of some other remedies was included in Menzie et al. [62] and can be shown in Figure 2-4.

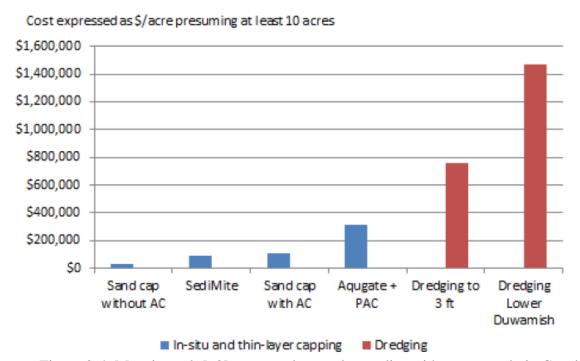


Figure 2-4. Menzie et al. [62] compared several remedies with a case study in Canal Creek, Maryland.

The other estimation based on the parameters from Kupryianchyk et al. [5] was made by the author and matched the results of Menzie et al. [62]. Kupryianchyk et al. [5] provided parameters including the material cost for thin layer capping: $3 \notin kg$; operational cost: $30 \notin m^3$; dredging cost: $1-10 \notin m^3$; the cost of thermal treatment: 60 €/m³; the cost of disposal: 10–20 €/m³. Assuming a contaminated site with pollutants within 50 cm deep; providing thin layer caps with 3.5 kg/m² (as suggested by Ghosh et al. [7]). Thus, a brief calculation on the cost of thin layer capping is approximately NTD\$4,800,000 per HA (with 87.5% of the material cost and 12.5% of operational cost). In terms of dredging and thermal treatment, a cost of NTD\$14,200,000–18,000,000 per HA were needed.

Based on the estimation of Kupryianchyk et al. [5] and Menzie et al. [62], a brief cost thin layer capping (about NTD\$5,000,000–6,000,000 per HA) is likely to be much cheaper to ex-situ treatment (various within NTD\$20,000,000–60,000,000 per HA). This estimation of dredging also be matched by NRC [91], which estimated the cost of dredging may be in between US\$145–530 per CY (NTD\$16,620,000–60,770,000 per HA). Although it should be fair to point out that some aspects may not be included, such as that the estimation based on Kupryianchyk et al. [5] only estimated the major portion of the thin layer capping (i.e. material cost and operational cost). Also, some other factors remain complex and can be site-specific, which is also not included in the estimation. As a whole, however, it can be fair to point out that the thin layer capping technology can be less costly compared to ex-situ methods if operated correctly.

2.6 Challenges and Opportunities

As demonstrated in the previous chapters, the thin layer capping technology is a promising alternative for the sediment remediation, but challenges remain in various aspects. Therefore, future studies are needed to fill in knowledge gaps as suggested below:

(1) In the field of material science, the relationship between sediment contaminants and the capping materials should be further studied. Although the sequestration of POPs by AC has been widely studied, the sequestration of other contaminants (e.g. Hg) that pose high threat to ecology and human health is also needed. Novel sorbents are needed to adopt different contaminants and various wetland conditions [14]. Also, the impact of various geochemical factors (e.g. dissolved organic matter, ions, microbial, or biotas) can have major roles in determining the success of the thin layer capping, and the interaction of which should be further studied.

- (2) In the field of geology, submarine groundwater flow [92], river erosion [17, 18], tidal effects [15, 16], and bioturbation [93] have been identified as critical mechanisms in contaminant transport in the natural aquatic environment. The stability and successfulness of thin layer capping under water can be determined by such geological condition. The research establishing the efficiency of thin layer capping with sediment turbation is scarce. One of the reasons may be due to the difficulty of simultaneously quantifying turbation magnitude [94, 95] and providing a comparable condition to real site capping application.
- (3) In the field of engineering and the real site practice, the anchoring problems for lighter materials (e.g. AC) sometimes results in settling problems or material loss [9]. The strategies such as the granulating materials, adding anchoring materials, or manufacturing materials into geotextile mat [96] may be useful but requires further studies.
- (4) In the field of ecology, some studies reported that the AC amendment did not result in ecological disturbance in field studies [70, 97, 98], while other found benthic biotas suffered from reduced species richness, biomass loss, reduced feeding rate, organ damage, or reduced growth after carbon amendment in labs

[70-72] or field sites [63]. The materials for thin layer capping should be put into tests before real site application.

(5) In the field of legislation and regulations, the bias against remedies other than removal still exists. There are also perceptions and regulatory precedents to "get it out". This view of sediment remediation may be appropriate but there are numerous occasions where removal is not realistic or ineffective for risk reduction [7].

Chapter 3 Capping of Mercury Sediment with SAC

3.1 Introduction



With high neurotoxicity, volatility, and bioaccumulation ability, mercury (Hg) has been considered as one of the most toxic heavy metal in the environment. Hg, in general, exists in the form of divalent Hg (i.e., Hg²⁺) in the aqueous phase and may transform to methylmercury (MeHg), which is one of the most toxic Hg forms via biomethylation under an anoxic sediment environment [2]. With high affinity in organism tissue [35], MeHg has high tendency to accumulate in biota and biomagnify through food chains, thus causing adverse effects to biota or human. Although ex-situ strategies have been proven promising in removing Hg out of sediment [3, 4], problems such as unfeasible cost [5], resuspension of contaminants [6, 7], and production of contaminated sediment residues [6, 7] may discourage their application. Therefore, development of novel and feasible techniques in remediating Hg-contaminated sediment is highly needed.

In-situ thin layer capping is a newly emerged in-situ remediation concept that can be apply to remediate Hg-contaminated sediment. Thin layer capping involves the use of active materials to sequestrate contaminant in sediment, therefore achieving remediation goal of reducing uptake of contaminants by biota and subsequently by the human. It has been shown that thin layer capping using activated carbon (AC) could be a promising treatment in reducing organic contaminant bioavailability in sediment, and has been demonstrated either in full-scale studies [8-10, 59, 61, 62] or long-term prediction models [48, 99]. As for Hg-contaminated sediment, however, fewer studies have been conducted [62, 66, 100], the reason may be because that AC generally has higher affinity to organic pollutants (log $K_D \approx 7.0-10.0$) than Hg (log $K_D \approx 3.0-7.0$) [64]. Therefore, seeking effective active materials with higher affinity to Hg is an important step to adopt the thin layer capping technique to Hg-contaminated sediment.

Sulfur-impregnated activated carbon (SAC) has been verified to enhance Hg adsorption capacity than its raw AC precursor in aqueous adsorption tests [12-14]. The results were reasonable considering its reaction thermodynamics, for which Hg has high affinity to sulfur (i.e., log K \approx 52.7–53.3) [23], as compared to that for Hg to organic matter (i.e., log K = 22–28) [35]. Wang et al. [12] demonstrated that an increase in Hg adsorption capacity of coconut AC from 150 to 820 mg/g by sulfurization with sulfur powder (C/S ratio: 1:2) was shown. Furthermore, Li et al. [13] increased Hg adsorption capacity of coke from 315.8 to 694.9 mg/g by impregnated the coke with sulfuric acid (80°C, 13 h).

Based on the previous research, we expected that SAC may have strong potential as thin layer capping material to remediate Hg-contaminated sediment. However, studies on using SAC as the thin layer capping material for inhibiting the release of Hg and MeHg from sediment environment are not done and presented. In this research, aqueous adsorption tests, sediment competition adsorption tests, and microcosm experiments were carried out to verify the Hg adsorption abilities of SAC and its raw AC counterpart. The feasibility of using SAC as the capping material for inhibiting the release of Hg and MeHg from sediment environment was further evaluated. The results obtained in this study are practically critical because a highly Hg-contaminated site in Southern Taiwan is currently remediated, for which thin layer capping has been considered as one of the feasible approaches for limiting the accessibility of biota to the Hg present in the contaminated seawater ponds.

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3.2 Materials and Methods

3.2.1 Materials



The actual sediment used in the study, designated as TY03, was sampled from Taoyuan irrigation channel, Taiwan, acquired according to the Taiwan Environmental Protection Administration (TEPA) standard method (NIEA S104.32B). Sediment within 0–15 cm depth was collected using a stainless crab bucket. Sampled sediment was immediately measured for oxidation-reduction potential (ORP) and then sealed in bags and transported back to the laboratory within 4 h. Wet sediment was air-dried in a laboratory hood, picked out branches and benthic biota, then ground and sieved to pass through 20 mesh sieve. Dry sediment was stored in room temperature without sunlight. Commercial AC was obtained as raw AC material (10–18 mesh). Received AC was first rinsed with DI water for several times and dried in 60°C for 24 h, then stored in a drying kettle. SAC was prepared by mixing 20 g of AC and 4 g of sulfur powder in a heating boat, heated to 400°C for 1 h and maintained for 2 h in a tubular furnace (Lindberg/Blue-M model STF55346C); 50 mL/min of nitrogen gas was constantly flowed through the furnace tube to maintain an oxygen-free environment. The prepared SAC was then sieved to 10–18 mesh and stored under the same condition as that for AC.

3.2.2 Physical and Chemical Analysis of Materials

Sediment pH was measured by pH meter (SunTex SP-2300) based on TEPA standard method (NIEA S410.62C); readings of pH value were recorded after adding 20 g of dried sediment and 20 mL DI water in a 50 mL beaker and set for 1 h. The texture of sediment was measured using a bouyoucos hydrometer [101]. The cation exchangeable capacity (CEC) of sediment was measured by available K, Na, Ca, and Mg, which were extracted

by leaching dry sediment through 1 N NH₄OAc solution, based on TEPA standard method (NIEA S201.61C). Other elements including Fe, Mn, Al, K, Na, Ca, and Mg were extracted by citrate bicarbonate buffer solution [102] and then measured by ICP-OES (Agilent 710 Series, Agilent Technology). Sediment organic content was measured through Walkley-Black wet oxidation [103]. The concentrations of NH₄⁺-N and NO³⁻-N were measured by steam distillation using MgO and the Devarda's alloy [104].

The specific surface area and pore size distribution of the adsorbents (AC and SAC) were measured using a physisorption analyzer (ASAP 2020M, Micromeritics Inc.). Nitrogen adsorption-desorption isotherm at 77K was obtained using a Micromeritics ASAP 2020; the Brunauer-Emmett-Teller (BET) method was used to determine the specific surface area at relative pressure (P/P₀) within 0.05 to 0.3 based on ASTM D4820-96a. Micropore size distribution was determined by the quenched solid density functional theory (QSDFT) model. The surface morphology of adsorbent was measured by a scanning electron microscope (SEM, JSM-7600F, JOEL). X-ray photoelectron spectra (XPS) were recorded using a ULVAC PHI-5000 VersaProbe spectrometer with monochromatic Al K α radiation. Element analysis was carried out by an elemental analyzer (Flash 2000, Thermo ScientificTM) to measure elements including C, H, O, N, and S in the adsorbents.

3.2.3 Aqueous Adsorption Experiment

The aqueous adsorption experiment was performed resembling Wang et al. [12] In brief, analysis-grade AAS Hg standard (1000 mg/L Hg, J.T.Baker) and MeHg standard (1 mg/L, BrooksRand) were used as Hg stocks and diluted to prepare Hg²⁺ and MeHg solution, respectively. Hg solution was adjusted to pH = 7.0 ± 0.1 using NaOH (0.01–0.1 M) and HCl (0.01–0.1 M) solution. Adsorbent (AC or SAC) of 50 mg and 50 mL Hg solution were added into clean 100 mL HDPE bottles. The HDPE bottles were then placed in a water bath shaker (30°C, 125 rpm). After the adsorption tests, water samples were collected for analysis of THg and MeHg.

3.2.4 Sediment Competition Adsorption Experiment

Hg-containing sediment in this study was prepared by spiking Hg solution in the sampled sediment. Hg stock solution (5000 mg-Hg/L) was prepared by dissolving HgCl₂ in DI water with 0.2% HCl. The spiking procedure was carried out by adding 200 g of dried sediment into a clean 400 mL glass jar; Hg stock was diluted with DI water and added to the glass jar to an anticipated Hg sediment concentration of 15–250 mg/kg. The glass jar was then filled with DI water, capped with stainless steels caps and sealed with parafilm. Spiked sediment jars were incubated for 117 d. After incubation, overlying water was removed, and sediment was freeze-dried and stored in a 4°C refrigerator.

Sediment competition adsorption experiments were carried out by adding 5 g of dried Hg sediment, 50 mg of adsorbent, and 50 mL of DI water in a HDPE bottle. The HDPE bottles were placed in the water bath shaker (30°C, 125 rpm) for 96 h. After the adsorption tests, water samples were collected, filtered through 0.45 µm mixed cellulose ester filter (DISMIC-25AS, Toyo Roshi Kaisha, Ltd), added 0.1% BrCl₂ solution and stored in glass bottles. Sediment samples and adsorbents were separated, freeze-dried, and sieved (20 mesh). Microwave digestion was then carried out using aqua regia to treat the sediment and adsorbent samples to obtain the aqueous aliquots for subsequent Hg measurement.

3.2.5 Microcosm Experiment

Vertical upflow microcosms were constructed in this study to measure the Hg release from sediment to its overlying water (Figure 3-1). Vertical microcosms were designed to have a total height of 30 cm with an internal height of 15 cm and an internal diameter of 6 cm and with glass fiber filter at the bottom. Tap water was initially filtered with MF filter and stored in a 20 L equalizer. Filtered water was then pumped into the columns as inflow fluid by a peristaltic pump with a flow rate of 1.0 mL/min.

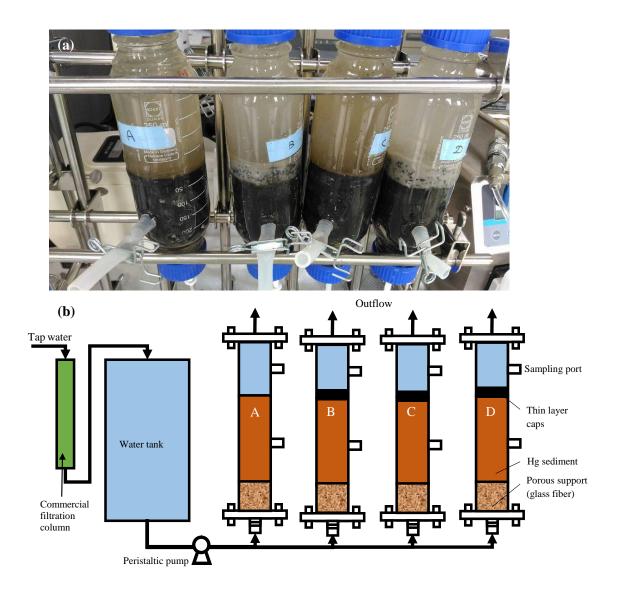


Figure 3-1. (a) photo image; (b) scheme diagram of vertical up-flow microcosms construction. Vertical flows were delivered from the bottom of the columns. The depth of sediment (TY03) is approximately 15 cm. From column A to D: (A) no caps; (B) SAC + bentonite; (C) SAC + additional TY03 sediment; (D) AC + bentonite.

Four columns were set in this study, with each column filled with 200 g of dried Hg sediment containing 250 mg-Hg/kg-sediment prepared as aforementioned. Active caps were deployed by mixing adsorbents with bentonite or clean sediment, described as follows. Column A was set with no caps as the control unit; column B was capped with the SAC (6 g; i.e. 3 wt% SAC added) and bentonite (6 g) mixture; column C was capped with the SAC (6 g; i.e. 3 wt% added) and bentonite (6 g) mixture; column D was capped with the AC (6 g; i.e. 3 wt% added) and bentonite (6 g) mixture. To start up microcosms, dried Hg sediment was added into the column and filled with filtered water for 24 h to settle, then the mixtures of active caps were gently added on top of the column and let the mixtures be settled to the surface of the sediment. After 1 h of settling, 1.0 mL/min flow was given and counted as the operation day 1. Outflows of the systems were carried out with tubing and the top of the column was sealed without headspace. Temperature, ORP, and pH value of the overlying water were measured constantly, and water samples for THg and MeHg analyses were collected weekly.

3.2.6 Mercury and Methylmercury Analysis

Water samples for THg and MeHg analyses were filtered through 0.45 μ m mixed cellulose ester filter (DISMIC-25AS, Toyo Roshi Kaisha, Ltd), then added 0.1% BrCl₂ solution (THg) or 0.2% HCl (MeHg) and stored in 50 mL glass bottles (THg) or 40 mL brown glass bottles with Teflon caps (MeHg), respectively. THg in sediment and water was measured following USEPA 1631 and NIEA W331.50B, and measurement of MeHg in sediment and water followed NIEA S341.60B and NIEA W540.50B. Before analysis, Hg in THg sample was oxidized to Hg²⁺ by stored with 0.1% BrCl. Halogens in THg sample were destructed by H₃NO₃·HCl, and final reduction of Hg²⁺ to Hg⁰ was completed by SnCl₂. The sample was purged and Hg⁰ was collected on a gold trap. After thermal

desorption, the Hg⁰ was injected to cold vapor atomic fluorescence spectroscopy (CVAFS; Brooks Rand Automated Total Mercury System). MeHg sample was buffered by citrate buffer, and MeHg was ethylated by adding sodium tetraethyl borate (NaBEt₄). Ethylmercury was volatile and thus carried through purge and trap system and analyzed by GC/CVAFS (Brooks Rand MERX Integrated Automated MeHg Analyzer). Quality assurance (QA) and quality control (QC) were checked by analyzing duplicate samples, quality control samples, and spiked samples from each batch.

3.3 Results and Discussion

3.3.1Characteristics of Sediment and Adsorbent

The characteristics of sediment (TY03) are listed in Table S3-1. TY03 had a pH value of 5.23 and soil organic content (SOC) of 3.66 wt%. Organic content in sediment is an important parameter for adsorption. As shown in previous research, SOCs of sediments have been observed as low as 1–2%, while can be as high as 15–20% [65, 105, 106]. Therefore, TY03 may be considered acidic sediment with relatively low organic content. THg of TY03 was averaged 0.6232 mg/kg. The texture of sediment can be categorized as sandy loam with sand, silt, and clay content of 73.6, 9.6, and 16.8 wt%, respectively.

The characteristics of adsorbent AC and SAC including BET surface area, total pore volume, median pore width, and element content (C, H, O, N, S) are shown in Table 3-1, indicating that the characteristic of ACs was different after sulfur treatment. Raw AC had a high specific area of 818.3 m²/g. After sulfurization, the BET specific area decreased to 728 m²/g for SAC. Similar results have been observed in several studies[12, 14, 41, 74]. Asasian and Kaghazchi [74] reported that sulfurization with elemental sulfur to coal-based AC resulted in a decrease in surface area by 58% (from 828 to 596 m²/g). Wang et

al. [12] also observed a marked decrease of surface area by 47% (from 1884 to approximately 1000 m²/g) as sulfurizing the coconut AC with elemental sulfur. In this study, only 10.9% of surface area were lost, the reason may be due to the large granular size (i.e., 10–18 mesh) of AC leading to less block and destruction of the internal porous structure of AC. Shifting of the average pore width toward a larger value and a decrease in total pore volumes were also observed after sulfurization of AC. Comparing the results from surface area analysis and SEM images (Figure S3-1), it may suggest that the reduction of surface area was mainly due to the collapse or block of micropores by heating and sulfur attachment. QSDFT micropore structure analysis (Figure 3-2) supported the reduction of micropores within a pore width of 0.5–1.0 nm after sulfurization. Additionally, the morphology of AC and SAC obtained by SEM images showed no significant difference in the surface structure after sulfurization.

Tables 3-1. Physical and chemical properties of precursor AC and resulting SAC.

| | BET surface area | Total pore volume | Mean pore width | С | Н | 0 | Ν | S |
|-----|---------------------|----------------------|-----------------|-------|------|-------|------|------|
| | (m ² /g) | (cm ³ /g) | (nm) | | | (wt%) | | |
| AC | 818.4 | 0.462 | 0.9454 | 78.88 | 1.41 | 4.52 | 0.73 | 0.47 |
| SAC | 728.1 | 0.416 | 0.9809 | 75.42 | 1.22 | 6.32 | 0.73 | 4.10 |

After sulfurization, the sulfur content increased from 0.47 to 4.09 wt%. This content was smaller compared to some SAC with sulfur content as large as 10–22 wt% reported in preview research [12, 74] because we intentionally kept the sulfur content less than 5 wt%. By doing so, most of the surface area and pore volume can be maintained because the pores were not markedly blocked by the impregnated sulfur. The sulfur content within

4–5 wt% should be sufficient for Hg capture with various sulfur functional groups in the SAC based on XPS results (Figure 3-3). The deconvoluted XPS S_{2p} signals at binding energies of 163.90, 164.75, 165.24, 166.36, 167.88, 168.67, and 169.41 eV corresponded to functional groups such as sulfide (C-S-C) + thiophene (C-S-C) + thioethers (C-S-C) + mercaptans (C-SH), disulfide (C-S-S-C), sulfinyl group (C₂S=O), sulfinyl group (C₂S=O), sulfone (C₂S(=O₂)), sulfone (C₂S(=O₂)), and sulfonate (C-SO₃) reported in previous studies[12, 107-109]. Hsi et al. [110] suggested that impregnated elemental sulfur would remain mainly as elemental sulfur groups on the surface of carbon in the heating condition of 250°C; as temperature increased to 650°C, increasing organic sulfur groups was observed.

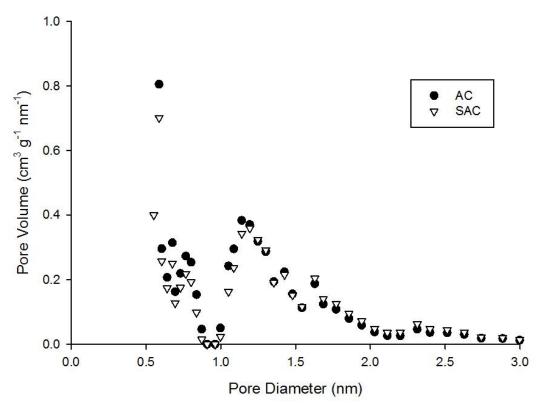


Figure 3-2. Micropores size distribution of raw AC and SAC based on QSDFT model.

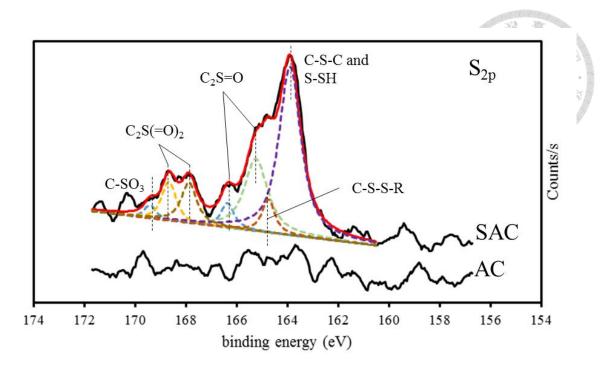


Figure 3-3. Deconvoluted S_{2p} peak for AC and SAC.

3.3.2 Aqueous Adsorption Experiment

Kinetic adsorption tests were carried out with Hg^{2+} adsorbed to AC and SAC (Figure 3-4). The experimental results suggested that about 81% of THg adsorption occurred within the first 6 h, with removal efficiency of Hg^{2+} at approximately 56.3 and 79.1% by AC and SAC adsorption, respectively. The equilibrium was reached at a time between 16 and 24 h. The adsorption rate appeared to be slower due to the larger size of granular AC (i.e., 10–18 mesh), as compared to previous research. For example, Li et al. [13] observed 87% of total Hg adsorption in the first 3 h, achieving equilibrium at around 10 h.

The experimental data were further fitted by pseudo-first and pseudo-second order kinetic models, for which the equations were described as below:

Pseudo-first order rate equations:

$$\frac{dq_t}{dt} = k_{S1}(q_e - q_t) \tag{eq. 1}$$

doi:10.6342/NTU201901399

$$log(q_e - q_t) = log(q_e) - \frac{k_{S1}}{2.303}t$$
Pseudo-second order rate equations:

$$\frac{dq_t}{dt} = k_{S2}(q_e - q_t)^2$$
(eq. 3)

$$\frac{1}{(q_e - q_t)} = \frac{1}{q_e} + k_{S2}t$$
 (eq. 4)

Whereas q_t = sorption of sorbate concentration on the sorbent at given time t; q_e = sorption of sorbate concentration on the sorbent at equilibrium state; k_{S1} =rate constant for pseudo-first order model; k_{S2} =rate constant for pseudo-second order model.

Pseudo-first and second order models can, therefore, being employed by eq. 2 and 4 to describe the adsorption data. The kinetic parameters were calculated and shown in Table 2-2. Both the adsorption data of AC and SAC had a better fitting to the pseudo-first order model (R^2 =0.9803 and 0.9827, respectively) than to the pseudo-second order model (R^2 = 0.9318 and 0.8636, respectively). The pseudo-first order kinetic constant for AC and SAC is 2.994×10⁻³ and 3.224×10⁻³ min⁻¹, respectively, indicating that SAC had a faster rate of reaching adsorption equilibrium than AC. This adsorption rate appears to be lower than previous research [13], but it is in prediction since the AC used in this research is granular (> 300 µm in diameter) rather than in powder (< 300 µm in diameter). Coarser AC has been long regarded slower and less effective in adsorption reaction as compared to finer AC [5, 9, 47]. Zimmerman et al. [47] discovered that GAC (400–1700 µm in diameter) was less effective in reducing hydrophobic organic contaminant bioaccumulation in one-month tests. Cornelissen et al. [9] compared different field tests and found that finer AC (<45 µm in diameter) showed higher adsorption effectiveness than coarser AC (75–300 µm in diameter) but less capping stability. Although slower

adsorption rate of GAC was observed in previous studies and in this work, it is still reasonable to use coarser GAC because it is more stable to serve as the thin layer capping material [9].

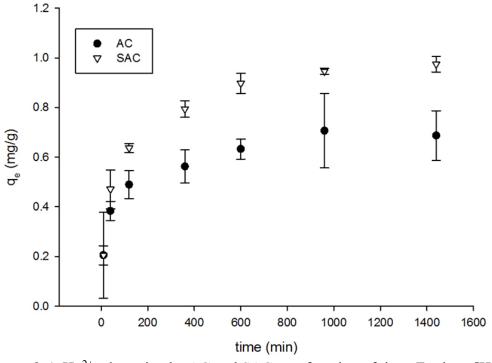


Figure 3-4. Hg^{2+} adsorption by AC and SAC as a function of time. For here $[Hg^{2+}] = 1$ mg/L, Hg solution = 50 mL, adsorbent dosage = 50 mg, and pH = 7.0±0.1.

| | | Pseudo-first order | | | Pseudo-second order | | | |
|------------|---------------|--------------------|----------------|----------------------|---------------------|----------------|-----------------|---------|
| Temperatur | e Hg | | q _e | k _{s1} | R_1^2 | q _e | k _{s2} | R_2^2 |
| | concentration | Adsorbent | | | I | | (-) | 2 |
| (°C) | (mg Hg/L) | | (mg/g) | (min ⁻¹) | | (mg/g) | (g/mg- | |
| | | | | | | | min) | |
| 20 | 1.0 | AC | 0.6232 | 0.002994 | 0.9803 | 0.5237 | 0.0249 | 0.9318 |
| 50 | | SAC | 0.8040 | 0.003224 | 0.9874 | 1.1130 | 0.0327 | 0.8636 |
| 30 | 1.0 | | | | | | | |

Table 3-2. Fitting parameters of AC and SAC adsorption by pseudo-first and second

order reaction models.



Distribution coefficient (K_D) is a useful tool to describe the affinity of Hg to AC [64, 65] in a linear relationship, defined as the ratio of the concentration of sorbate sorbed to the sorbent divided by its concentration in solution. This concept includes an assumption that the solute concentration is very low that the sorption of sorbent only controls by concentration of solution rather than remaining sorption sites on the sorbent. It was recently discovered that the distribution of adsorbate on black carbon should be considered with two separated mechanisms (adsorption and partition) [111], and by definition, Hg uptake by black carbon should be mainly governed by adsorption mechanism because Hg uptake capacity does not increase after reaching maximum capacity, which was observed in previous research [13, 73, 74]. However, it may still be plausible to introduce K_D concept since the Hg concentration used in this study was very low and far from reaching the maximum adsorption capacity of AC.

Adsorption isotherms of AC and SAC are shown in Figure 3-5. The results showed that K_D of SAC (9.426×10⁴, R²=0.996) to Hg²⁺ was more than two-fold larger than that for AC (i.e., 3.694×10⁴, R²=0.958). Notably, the affinity of ACs to MeHg was almost 10times larger than that to Hg²⁺, as shown in our results, that K_D for AC and SAC to MeHg was 2.254×10⁵ (R²=0.983) and 7.661×10⁵ (R²=0.834), respectively. The reason for SAC having greater adsorption affinity to Hg²⁺ than AC is expected. As aforementioned, Hg can be immobilized by sulfide to form highly stable HgS (i.e., log K ≈ 52.7–53.3) [23]. SAC had larger sulfur content (4.09 wt%) than that of AC (0.47 wt%). Additionally, based on the XPS results, SAC possessed various sulfur functional groups; all of which lead to the higher affinity to Hg²⁺ for SAC than for AC [12, 13, 74]. On the contrary, results of AC and SAC having higher affinity to MeHg than Hg^{2+} in this work is not completely consistent with those from previous studies. Gomez-Eyles et al. [64] compared K_D of various black carbons to MeHg and Hg and found that six materials with Hg K_D to MeHg K_D ratios significantly greater than one, two materials with the ratios close to one, and six materials with the ratios significantly smaller than one. These results may suggest that adsorption of Hg^{2+} and MeHg involves different mechanisms.

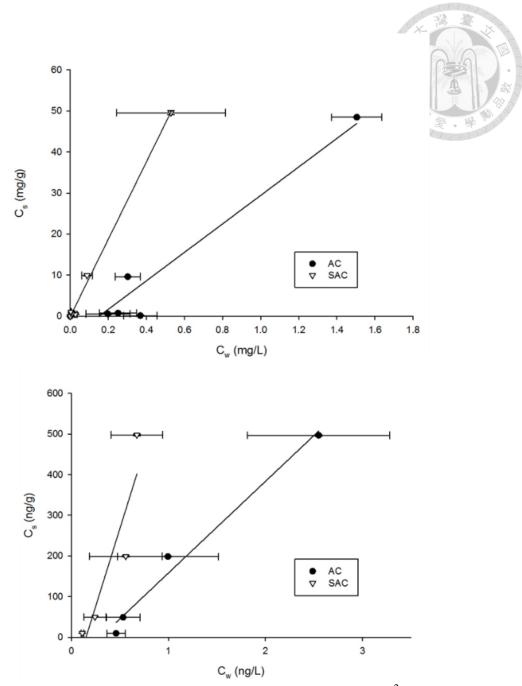


Figure 3-5. Adsorption isotherm of AC and SAC adsorbing (a) Hg^{2+} and (b) MeHg.

Adsorption time = 24 h. Hg solution = 50 mL, adsorbent dosage = 50 mg, pH = 7.0 ± 0.1

3.3.3 Sediment Competition Adsorption Experiment

Three spiked Hg-containing sediments with Hg content of 14.23, 106.28, and 235.78 mg/kg were prepared by 117-d incubation, and the sediment/adsorbent competition adsorption tests were carried out by measuring Hg concentrations in the sediment and porewater for 1, 3, and 6 wt% activated carbon addition, which is shown in Figure 3-6. Under the condition of 1 wt% adsorbent dosage (Figure 3-6a), porewater THg was reduced by 73.4–96.2% by AC and 83.25–95.21% by SAC in the sediment with Hg range of 14.23–106.28 mg/kg. The decrease of effectiveness at 235.78 mg/kg may be due to reaching the equilibrium adsorption capacity of AC and SAC. At 3 wt% adsorbent amendment (Figure 3-6b), AC reduced 91.9–99.9% porewater THg in the Hg sediment range of 106.28–235.78 mg/kg, while SAC reduced 86.4–90.5% porewater THg. Notably, at the adsorbent dosage 3–6 wt%, the enhancement in porewater THg reduction was less obvious as compared to the dosage from 1–3 wt%.

Surface water Hg concentration of 1.3 μ g/L was set by Preliminary Remediation Goal (PRG) for an ecological endpoint [112], and 3 wt% dosage of AC can cause porewater THg concentration beneath this level throughout the tested sediment Hg range in this study. It indicates that 3 wt% of AC or SAC could be an optimum dosage for thin layer capping remediation of Hg sediment with wide Hg concentration range up to 235.78 mg/kg, in terms of amount and cost as compared to amending 6 wt% adsorbent.

Surprisingly, amendment of SAC led to lesser porewater THg reduction as compared to that of AC, especially at the dosages of 3 and 6 wt%, which is inconsistent to the results obtained from our batch-scale aqueous adsorption tests aforementioned. Notably, for the sediment with Hg content of 14.23 mg/kg, 1 wt% of SAC addition significantly reduced porewater Hg to 83.3%; but with the amendment of 3 and 6 wt%, the reduction ratio was

only –31.3 and 6.4%, respectively. The reason of the inconsistency is not yet thoroughly understood, but may be attributed to the elongation of adsorption time (from 24 to 96 h) and the influence of inherent components in sediment leading to the instability of HgS complexes on the SAC surface. However, this possibility can be ruled out by a follow-up test (Figure S3-2) showing that no obvious Hg was re-dissolved in the aqueous phase for up to 72 h, and no aggregation was observed by measuring the aqueous samples filtered by different pore-sized membranes.

Another reason causing the lesser porewater THg reduction by SAC may be due to the re-dissolution of HgS_(s) nanoparticles after adsorption on SAC, triggered by sediment. This mechanism has not yet reported but is reasonable in explaining the inconsistency of aqueous adsorption and sediment competition adsorption experiments in this study. Hg is well-known to have high affinity to sulfur. However, the formed fine particles of HgS_(s), via interaction of Hg with impregnated elemental sulfur present in SAC surface, may dissolve again into Hg²⁺ and SO₄²⁻ in an oxic environment [113, 114]. In addition, as sulfur exists in an aqueous environment, Hg²⁺ and S²⁻ could precipitate and form β -HgS_(s) nanoparticles at sulfur concentration even as low as 1 nM [23]. Without interference, β -HgS_(s) nanoparticles would gradually aggregate forming larger particles with a diameter of 200–500 nm [114]. However, when the aqueous environment exists dissolved organic matter (DOM), the aggregation of β -HgS_(s) nanoparticles may be inhibited and even redissolved to the aqueous phase [115].

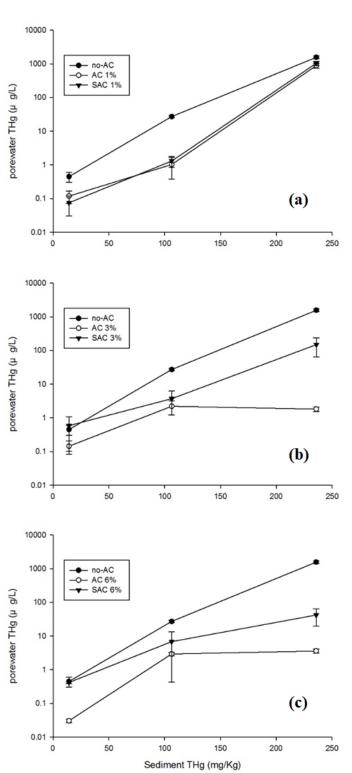


Figure 3-6. Hg concentrations in porewater versus in sediment at (a) 1 wt%; (b) 3 wt%; (c) 6 wt% adsorbent addition based on sediment competition adsorption test. DI water is 50 mL and Hg sediment is 5.0 g.

As aforementioned, SAC had higher Hg²⁺ and MeHg affinity compared to AC based on aqueous adsorption tests and the reason was attributed to the stable bonding of Hg-S. As reported by Liu et al. [116], Hg has high tendency to bind to carbon-sulfur functionality such as C-S-S-C, C-S-C, and C-SH, which are abundant in SAC based on the XPS examination. However, in the sediment adsorption experiments, as the adsorption time increased from 24 to 96 h, with the possible release of DOM from sediment, sulfur functional groups may be destructed and dissolved, thus causing the Hg to form Hg-S-DOM cluster, as proposed in Figure 3-7. Consequently, The porewater THg reduction by SAC amendment was less pronounced as compared to that by AC amendment.

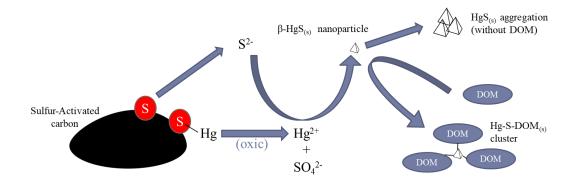


Figure 3-7. Proposed adsorption/desorption mechanisms of Hg adsorption on SAC in the sediment environment.

Although a similar phenomenon was observed previously, this is the first study to report the potential sulfur release from sulfur-impregnated activated carbon during sediment competition adsorption tests causing an increase in porewater Hg concentration. Liu et al. [116] also reported the SO_4^{2-} released from biochar causing Hg adsorption ability to decrease in a 48 h adsorptions tests. Similarly, Liu et al. [117] conducted

microcosms experiments and discovered that the release of Hg may have a high correlation to aqueous parameters such as the concentrations of Fe ions, SO_4^{2-} , and DOC. The influence of these parameters on Hg release from AC and SAC should be further comprehended.

3.3.4 Microcosm Experiment

During the 86-d microcosms operation, pH, ORP, temperature, and flow rate were recorded (Figs. S3-3–S3-6). In brief, the temperature of microcosms was maintained at around 25°C, pH value was typically in the range of 6.6–7.0, with few exceptions at the range of 6.2–7.4. Original ORP was around -200 to -300 mV after the operation started, ORP was dramatically increased and maintained at around 0–100 mV due to the supplied water had greater ORP.

Overlying water THg and MeHg concentrations of microcosms during operation are shown in Figure 3-8. As soon as the active caps deployed, a dramatic decrease of overlying water THg concentration by 91.2–95.9% (not shown in the graph) and MeHg (77.8–99.8%) in capped microcosms was observed at day 2. Throughout the operation period, the influence of caps to overlying water THg concentration was insignificant between days 17 and 47. While after day 47, THg started to leach and caused high amount of Hg in overlying water, with the highest THg concentration at day 63 recorded at 0.791, 0.281, 0.654, and 0.417 μ g/L for those from column A (control), column B (SAC+bentonite), column C (SAC+TY03), and column D (AC+bentonite), respectively. These leaching processes were also observed in Liu et al. [117] as leaching of Hg occurred at around day 80, with high correlation with the rising of Fe and SO₄²⁻ concentrations. Notably, previous studies have shown that re-dissolution of Hg-S complexes into Hg²⁺ and SO₄²⁻ may occur in an oxic environment [113, 116]. Therefore, with the increase of

ORP in our microcosms, the adsorbed Hg may be re-dissolved into the aqueous phase, which may partly lead to the increase in THg concentration after 47 d of operation time, especially for Columns A (control) and D (AC + bentonite) (Figure 3-8).

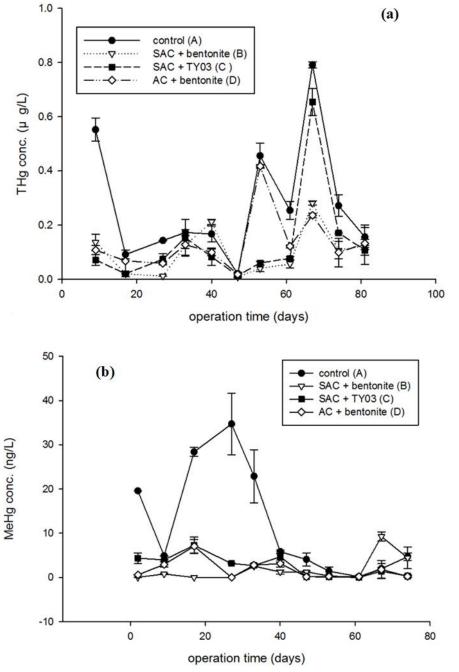


Figure 3-8. Overlying water (a) THg and (b) MeHg concentrations of vertical up-flow microcosms during operation.

Compared to THg, different inhibition patterns of MeHg into overlying water were observed in microcosms. As in the first 40 d, the sediment without active cap had high overlying water MeHg, with the highest concentration recorded as 34.7 ng/L. This value was 13 times higher than the Preliminary Remediation Goal set for the ecological endpoint (i.e., 2.6 ng/L) [112]. Microcosm results also showed that the presence of active caps had great leaching inhibition ability to MeHg, with MeHg reduction efficiency of higher than 79.1%. After day 60, all microcosms had relatively low MeHg, it may be due to increasing ORP in the system, causing microbiome shift, thus reducing biomethylation.

The microcosm results further demonstrated that using SAC or AC as thin layer capping can reduce the overlying water concentration of MeHg to a level far below ecology threat consideration, thus is applicable in reducing the risk from Hgcontaminated sediment since MeHg is the most toxic species of Hg.

3.4 Summaries

Feasibility of using raw and sulfur-impregnated activated carbon (SAC) for remediation of Hg sediment was evaluated. Prepared SAC had high porosity with efficient micropores, and sulfur on SAC was insufficient content and with various forms. Aqueous Hg adsorption results indicated that SAC had higher affinity to both Hg^{2+} and methylmercury (MeHg) compared to the raw AC precursor in 24 h of equilibrium time. However, as compared to the results from sediment competitive adsorption tests, the Hg adsorption performance of SAC was reduced with elongation of adsorption time, and possibly by the presence of certain components in the sediment environment leading the release of Hg. Fe ions, SO_4^{2-} , and dissolved organic matter have been reported and could cause marked impacts on Hg sequestration; therefore should be further clarified. Microcosm studies showed that all combinations including SAC+bentonite, SAC+TY03,

and AC+bentonite caps had good efficiency in reducing the MeHg concentration of overlying water. In contrast, active caps did not show corresponding high effectiveness in reducing the overlying water THg. Again, the release of Hg may stem from the redissolution of formed Hg-S complexes in SAC and need to be further examined.

SAC shows higher affinity toward Hg²⁺ and MeHg in short-term aqueous experiments than raw AC; nevertheless, sulfur-containing adsorbents do not necessarily enhance inhibition of Hg release from the sediment environment. In desire of applying SAC or other thiol-functionalized materials to thin layer capping, one should carefully evaluate the long-term effects in the complex conditions. A thorough examination on the stability of various sulfur functional groups on SAC as they interact with Hg species under aqueous sediment environment containing various components should be further conducted.

3.5 Supporting Information

| Sediment Code | TY03 | · · · · · · · · · · · · · · · · · · · | | | |
|-------------------------------|---------------------|---------------------------------------|--|--|--|
| Water content | 2.70±0.00 wt% | | | | |
| Sand | 73.6±0.6 wt% | | | | |
| Silt | 9.6±0.1 wt% | | | | |
| Clay | 16.8±1.6 wt% | | | | |
| рН | 5.23±0.01 | | | | |
| ORP | -93.2 mV | | | | |
| SOC | 3.66±0.09 wt% | | | | |
| CEC | 34.66±0.47 cmol/kg | | | | |
| Available NH4+-N | 0.273±0.001 mg/g | | | | |
| Available NO3 ⁻ -N | 0.0054±0.0003 mg/g | | | | |
| Fe | 49.67±2.61 mg/g | | | | |
| Mn | 0.39±0.04 mg/g | | | | |
| Al | 6.36±0.34 mg/g | | | | |
| K | 3.97±0.17 mg/g | | | | |
| Na | 3.03±0.60 mg/g | | | | |
| Ca | 4.81±0.60 mg/g | | | | |
| Mg | 0.20±0.05 mg/g | | | | |
| Hg | 0.6232±0.0089 mg/kg | | | | |

Table S3-1. Characteristics of sediment TY03 sampled from a river in Northern Taiwan.

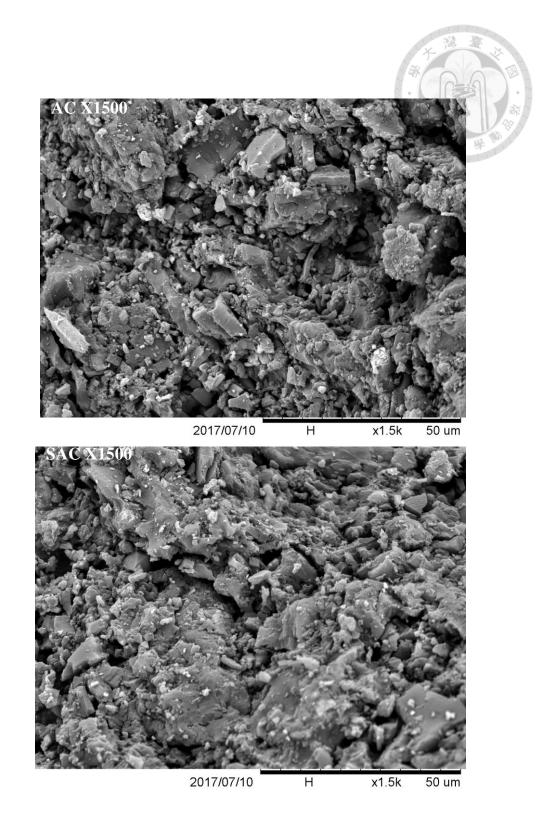


Figure S3-1. SEM images of raw AC and AC after sulfurization (i.e., SAC) under x1500 magnification.

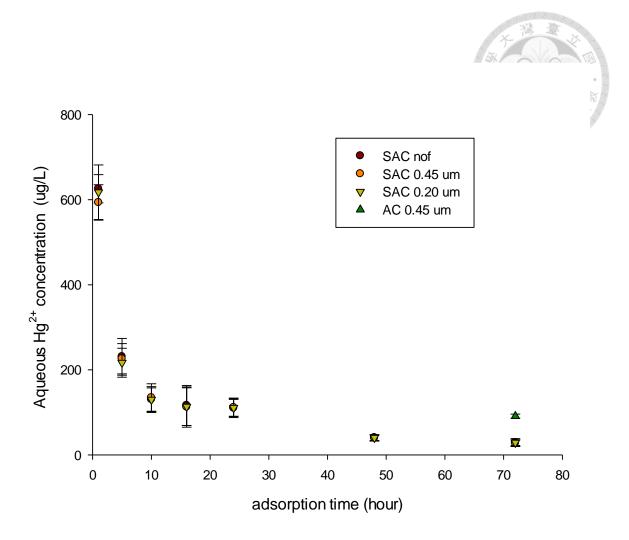


Figure S3-2. Follow-up aqueous adsorption tests of AC and SAC to justify the discussion in Section 3.3. The adsorption condition is as the same as the aqueous adsorption tests described in Section 2.3. $[Hg]_0=1 \text{ mg/L}$, Temperature = 30°C, 125 rpm, n = 3. Adsorption time was extended to 48 h and 72 h. Aqueous samples obtained with different pore-sized filtration are compared. SAC: sulfurized activated carbon; AC: raw activated carbon; "nof": no filtered treatment after adsorption test; "0.20": 0.20 µm filtered treatment; "0.45": 0.45 µm filtered treatment.

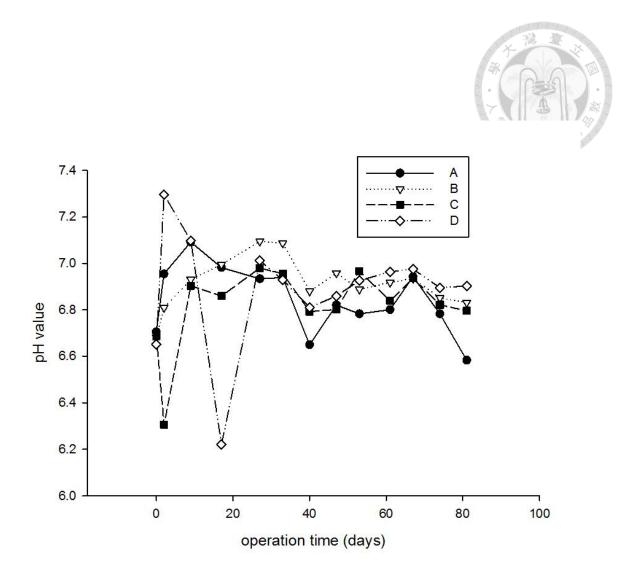


Figure S3-3. pH value variation of four vertical up-flow microcosms (A–D) during the operation of 86 days. From column A to D: (A) no caps; (B) SAC + bentonite; (C) SAC + additional TY03 sediment; (D) AC + bentonite.

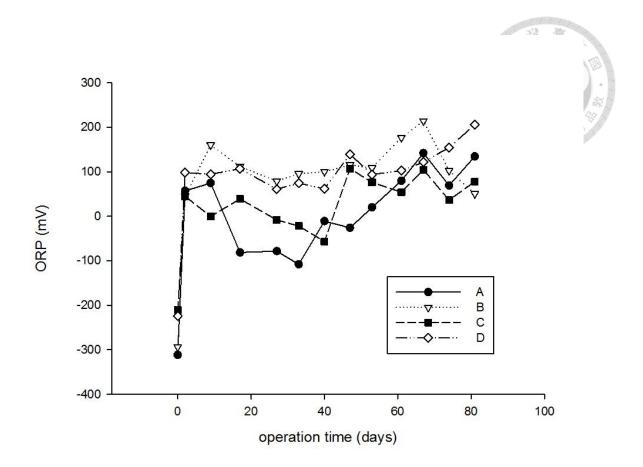


Figure S3-4. ORP variation of four vertical up-flow microcosms (A–D) during the operation of 86 days. From column A to D: (A) no caps; (B) SAC + bentonite; (C) SAC + additional TY03 sediment; (D) AC + bentonite.

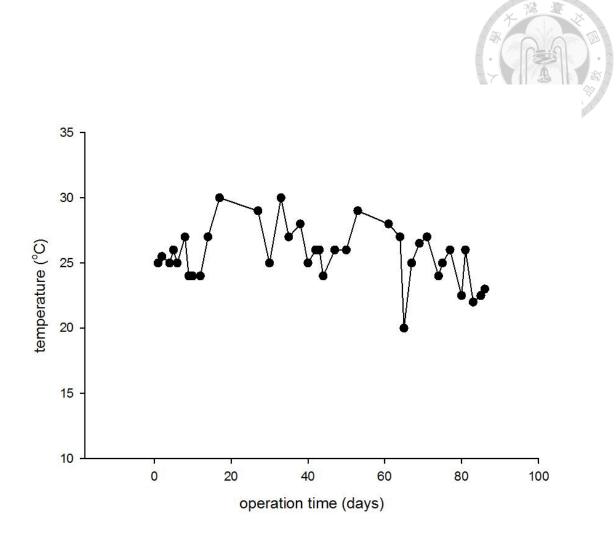


Figure S3-5. Temperature variation of four vertical up-flow microcosms (A–D) during the operation of 86 days. From column A to D: (A) no caps; (B) SAC + bentonite; (C) SAC + additional TY03 sediment; (D) AC + bentonite.

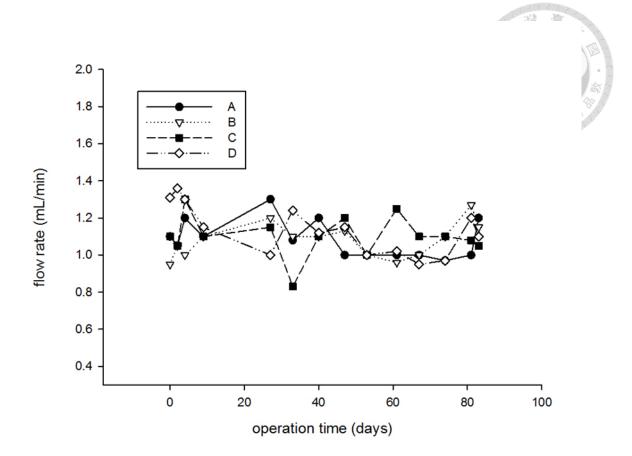


Figure S3-6. Flow rate variation of four vertical up-flow microcosms (A–D) during the operation of 86 days. From column A to D: (A) no caps; (B) SAC + bentonite; (C) SAC + additional TY03 sediment; (D) AC + bentonite.

Chapter 4 AC/clay-based Caps Reduce Mercury Escape under Horizontal Flows and Sediment Turbation

4.1 Introduction

Over decades, anthropogenic mercury (Hg) in the aquatic environment has been posing severe contamination and put the health of the environment biotas and human beings into risks. Wastewater discharge from industries (i.e. chlor-alkali and metallurgy) was particularly hazardous and has resulted in legacy Hg contamination in wetlands or estuaries worldwide [15, 27]. Although the sediment underneath water body acts as an ideal sink to retain Hg [16, 17] sediment-to-water Hg flux may continuously occur [93, 118] by occasional turbation events [15-18]. Sediments also provide an anoxic environment, facilitating the production of methylmercury (MeHg), which is a potent neurotoxin with a high bioaccumulative ability [119]. Consequently, Hg in contaminated sites was found entering the food webs and being biomagnified to each trophic level [119, 120].

In recent years, in-situ thin layer capping has emerged as a promising remediation approach as an alternative for solving the Hg contamination problems[64-66, 68, 69]. The success of applying thin layer capping to persistent organic pollutants (POPs)contaminated sediment [8-11] has also shed light on the Hg-contaminated sediments. The feasibility of applying thin layer capping with black carbon (BC) to the Hg-contaminated sediment remediation has been evaluated in various bench-scale studies [64-66, 69, 121] and field-scale studies [8, 68]. Several BCs were found to have efficient sorption affinity to either inorganic Hg (log $K_D = 3.0-7.0$) or MeHg (log $K_D = 3.0-5.0$) within a certain Hg concentration range [64, 121]. Also, reduction of Hg bioaccumulation in biotas [62, 65, 66] and porewater Hg [62, 65, 66, 121] was observed with BC application.

Although thin layer capping with BCs was found generally efficient in reducing Hg mobility and bioavailability, some major concerns including the capping stability and the potential risks of Hg escape from caps have been addressed [66, 68, 121]. The sediment turbations caused by bioturbation or physical erosion (e.g., tidal effect and temporal oxidation effect) have been identified as critical mechanisms in contaminant transport in the natural aquatic environment. Multiple studies have noted that inorganic Hg and MeHg were carried by fine-grained sediment from river erosion [17, 18] and tidal effects [15, 16]. Temporal oxidation event in sediment was also observed to cause Hg remobilization [121, 122].

It is intriguing how sediment turbation may affect the efficiency of the thin layer capping in treating Hg-contaminated sediment, but related studies remain little information. One of the reasons may be due to the difficulty of simultaneously quantifying turbation magnitude [94, 95] and providing a comparable condition to real site capping application. For these purposes, microcosm tests were carried out in this study to establish the crucial connection between capping stability and Hg immobilizing efficiency with sediment turbation.

4.2 Materials and Methods

4.2.1 Sorbents Preparation, Sediment Collection, and Characterization

A commercial granular AC (10–18 mesh) was selected and has been confirmed with efficient Hg sorption and leaching inhibition [121]. Bentonite, kaolin, and montmorillonite were purchased from Sigma-Aldrich[®] (CAS no. 1302789, 1332587, and

1318930, respectively). The Hg-contaminated sediment, designated as ANS, was collected from an estuary pond in a former chlor-alkali plant, the An-Shun Plant of China Petrochemical Development Corp., Tainan, Taiwan. The sediment within 0–15 cm depth was collected using a stainless crab bucket. Surface water in the same pond was also collected. Both sediment and water were transported to the laboratory (<10 h) and stored in room temperature without sunlight. Sediment was air-dried in a hood, picked out branches and benthic biotas, and ground and sieved (20 mesh). The pH and organic content of ANS sediment were 7.52 \pm 0.03 and 0.80 \pm 0.65 (wt%), respectively, indicating that ANS was a mildly alkaline organic poor estuary sediment (Table S4-1). The texture of pre-treated ANS belongs to sandy loam, and total Hg (THg) level was measured to be 76.0 \pm 2.593 mg/kg (Figure S4-1, Table S4-1). The electrical conductivity (EC), pH, total Fe, sulfide, sulfate, chloride, THg, and MeHg of the ANS surface water were also measured (Table S4-2).

4.2.2 Artificial Vibration System

A lab-made vibration system was designed to remobilize the thin surface layer, few millimeters from the top of the sediment, in which the depth may be comparable to bioturbation [94] or tidal movement [123] in short timescale. The system was composed of commercial brushless DC vibration motors (Figure S4-2; RISUN PVN 1305D 3V) and a lab-made current controller (Figure S4-3). The motors were coated with 2–3 layers of Hg-free epoxy resin and plastic steel for waterproof (Figure S4-2). Motors were tested to create 34.2 mA of current under 3.0 V. The power output was estimated to be 102.6 mW for each motor.

During the operation of the microcosm, five motors were placed in equidistance of 6 cm to each other in each cell (Figure S4-4) and the voltage was set to 3.0 ± 0.2 V by the

controller. The total power was thus estimated to be 513 mW per cell, giving bulk turbation magnitude of 12.8 W/m^2 . Every motor found malfunctioned was replaced within a week and recorded (Table S4-3).

It would be arbitrary to conclude this vibration system a perfect method to produce quantifiable sediment turbation, especially when more sophisticated and precise methods [95] or models [94, 124] exist. However, previously developed methods may find difficulty in applying to a more complex system. The vibration system in this study may provide a viable and straightforward method for sediment turbation quantification in a more complex system.

4.2.3 Microcosms Setup and Operation

The microcosm was composed of four cells (A, B, C, and D) (Figures S4-4 and S4-5). Cell A was set without a cap as the control unit; cells B, C, and D were set with thin layer caps application (around 1.5 cm thick) composed of AC (3%; 105 g) + bentonite (3%; 105 g), AC (3%) + kaolin (3%), and AC (3%) + montmorillonite (3%), respectively. Each cell was composed with an open canal segment $(50 \times 10 \times 10; 1 \times w \times h; cm^3)$ on top of a sediment tank segment $(40 \times 10 \times 10 \text{ cm}^3)$. The microcosm was designed to fill the sediment tank with 3.50 kg dry ANS sediment to approximately 9.0 cm in depth. The overlying water in the microcosm was introduced by the stored ANS surface water and set to 8.5 cm height in the open canal segment. Marks were made to locate the water line. The circular flow in each cell was carried by PE tubing, driven by a commercial submerged pump (Eden 105) in a PP water tank (1 L). The flow rate in each cell was corrected initially to 5 L/min (bulk velocity in microcosm = 58 cm/min). Also, the supplement of the overlying water was made daily by adding ANS surface water (due to sampling) or deionized water (due to evaporation or other loss) to the water line mark, maintaining the unity of the water properties. A rectifier was provided by a plastic net bag with 200 g of ceramsite and was fixed at the inlet of overlying water in each cell. A black box was constructed around the microcosm, and the light was provided by two aquarium LED lights (10 W each) and set to a 14:10 h, light:dark cycle.

The microcosm was established before the trial (i.e., recorded as day -98) allowing the aging of the sediment (Figure S4-6, Table S4-3). The trial started (day 1) as the artificial vibration system was placed in each cell (5 motors per cell; -12.8 W/m² in each cell). The microcosm stabilized for days, then thin layer caps were applied (day 12) with materials aforementioned after sediment was sampled. Capping materials were premixed in ANS surface water and applied to sediment surface evenly. The horizontal flow and turbation were stopped overnight allowing caps to settle. An intermittent turbation test was carried out by stopping the vibration system during day 20–31.

4.2.4 Sample Collection and Analysis

During the trial, temperature and dissolved oxygen (DO) were measured weekly. Overlying water of each cell was sampled and filtered (0.45 μm) each week. The room temperature of the microcosm was measured by a thermometer. DO of the overlying water was directly measured by a DO meter (EXStik[®], DO600). pH, EC, total Fe, sulfide, sulfate, and chloride of the water samples were analyzed immediately after sampling. pH value was measured by a pH meter (SunTex SR-2300). EC was measured by a conductivity meter (6021, EZDO). Sulfide, sulfate, chloride, and total Fe was measured by an ultraviolet spectrophotometer (Spectroquent® Prove 600, Merck) with kits (Catalogue no. 114779, 114548, 114897, and 100796, respectively). The detection limits of total Fe, sulfide, sulfate, and chloride were 0.05, 0.05, 5.0, 2.5, and 5.0 mg/L, respectively. The oxidation-reduction potential (ORP) of sediment with a depth of 1–3 cm of thin layer caps was measured by an ORP meter (SunTex SR-2300). The measurement was prosecuted by inserting the sensor of the ORP meter in the depth of 1-3 cm and stabilized for 2 h. Sediment was sampled 1-3 cm depth under sediment layer (not account for cap layer), stored at -20°C before subsequent analysis. The sediment measurement was controlled at fixed position in each cell (34 cm from the front; Figure S4-4). Although the sediment can be highly heterogeneous can may affect the results, careful measurement and triplicated sampling was prosecuted.

Overlying water for THg analysis was stored with 0.1% BrCl solution (< 1 week). Sediments for THg analysis were freeze-dried and digested (95–120% recovery). THg concentrations were determined following USEPA Method 1631 using BrCl oxidation, SnCl₂ reduction, purge and trap, and cold vapor atomic fluorescence spectroscopy (CVAFS; Brooks Rand Automated Total Mercury System) (85–100% recovery). Water samples for MeHg analysis were stored with 0.1% HCl solution in dark (< 2 d). MeHg was measured by distillation and ethylation, purge and trap and GC/CVAFS (Brooks Rand Automated Total Mercury System) by USEPA Method 1630 (water) and Taiwan-EPA method NIEA S341.60B (sediment) (93–115% and 93–110% recovery, respectively). QA/QC was checked by analyzing duplicate samples, quality control samples, and spiked samples from each batch.

4.3 Results and Discussion

4.3.1 Microcosms Operation

The combination of horizontal flow and artificial turbation has resulted in a visible suspension in the microcosm (Figure S4-7). Without turbation, no suspension was observed during the pre-test (Figure S4-6). A similar observation was reported by Xie et

al. [93] as the flow and bioturbation enhance sediment suspension. As anticipated, the overlying water of the control was highly turbid throughout the trials, likely caused by the fine particles released from the uncovered sediment surface. The AC + bentonite and the AC + kaolin caps were found successful to inhibit sediment resuspension as the overlying water was found less turbid than the control. However, the AC + montmorillonite was observed with high turbidity in overlying water comparable to the control, indicating that montmorillonite was less stable as compared to kaolin and bentonite. The reason may be that montmorillonite is a 2:1 type clay mineral and was considered efficient to absorb large amounts of water in the interlayer space [125]. To further inference, bentonite consists chiefly of one or more members of the smectitegroups (montmorillonite) minerals [126], therefore should also be possible to absorb water and become labile when applied as thin layer caps. However, AC +bentonite shown quite stable under turbation. This may be because that bentonite is a non-pure material consists of complex minerals, thus may help to stabilize the cap. Different from bentonite and montmorillonite, kaolin is a 1:1 type clay minerals, therefore may not be labile due to water sorption. In terms of Hg sorption capacity, bentonite (<1 mg/g [127]), kaolin (< 1 mg/g [128]) and montmorillonite (< 10 mg/g [129]) were known to have much lower sorption capacity as compared to coconut AC (~150 mg/g [12]). Therefore, the mechanism for the clays to inhibit sediment resuspension should be by forming barriers to block fine sediment particles.

The temperature in the microcosm throughout the experiment was stable at 25 ± 1 °C (Figure S4-8a, Table S4-4) with a few exceptions. DO in the overlying water was also stable between 6.0 and 7.0 in all cells throughout the trials (Figure S4-8b). The aeration may be caused by the little waterfall created by the reflux water in the PP tanks. This

value matches the An-Shun real-site conditions, as the overlying water in the estuary ponds was shallow and highly aerated. The pH value of overlying water in all cells was between 8.0 and 8.3 (Figure S4-8c) and is comparable to ANS surface water (Table S4-2).

EC in the overlying water was around $3.0-4.0\times10^4 \,\mu$ S/cm (Figure S4-8d), partially lower than that in ocean water (approximately $5.0\times10^4 \,\mu$ S/cm). After the thin layer caps application, a decrease of EC in the AC + bentonite and the AC + kaolin was observed to be $2.0-2.5\times10^4 \,\mu$ S/cm. In contrast, EC of the AC + montmorillonite remained comparable to that in the control, probably because of the lower capping stability (Figure S4-7). This result may indicate that the salt mud (originated from chlor-alkali brine (O'Brien et al. 2007)) was released to the overlying water as the turbation occurred. Thin layer caps may form the barrier thus reducing partial salt released from sediment.

4.3.2 Sulfide, Sulfate, Chloride, and Total Fe in Overlying Water

Sulfate, chloride and total Fe in the overlying water were measured throughout the study (Figure 4-1, Table S4-5). Sulfide concentration in the microcosm was smaller than the detection limit (<0.05 mg/L) throughout the operation. The reason may be the aerated condition in the overlying water causing sulfide re-oxidized to sulfate as released from the sediment, therefore, existed in a small concentration [130]. However, sulfide may still have a profound impact on Hg speciation even as low as 1 nM [23].

Sulfate, chloride, and total Fe in the overlying water in all cells were generally larger than those in the ANS surface water (Figure 4-1, Table S4-2), indicating that the ions measured were concentrated in the sediment and escaped to the overlying water by sediment-to-water flux.



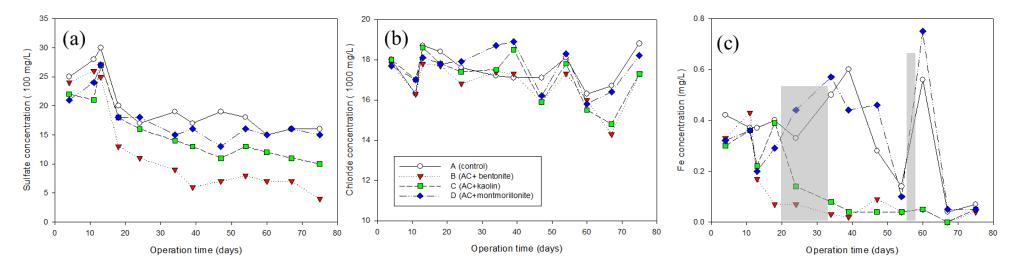


Figure 4-1. (a) Sulfate, (b) chloride, and (c) total Fe concentration in the overlying water of four cells of the microcosm. The gray bar between day 20 and 30 represents intermittent turbation test; the gray bar at day 54 represents the sediment sampling event.

The pattern of sulfate in overlying water (Figure 4-1a) was approximately 2.0-2.5×10³ mg/L and found positively correlated ($R^2 = 0.5950$; 0.4229≤ R^2 ≤0.7671 under 95% confidence level) to EC (Figure S4-9). This result indicates that sulfate may contribute to a large portion of EC that was concentrated in the sediment. Both the AC + bentonite and the AC + kaolin caps were found to decrease sulfate concentration in the overlying water significantly as compared to the control. In contrast, the AC + montmorillonite cap was not favorable for the sulfate reduction. Previous studies have found sulfate sorption behavior for bentonite [131] and kaolin [132]. However, it was suggested that montmorillonite has the permanent negative charge in silica structure [125], therefore could be unfavorable for sulfate sorption. Also, sulfate concentration was observed to gradually decrease in all microcosms. The reason behind may be that the overlying water was gradually diluted by the ANS surface water, which had lower sulfate, during every water sampling events (200 mL/cell).

Chloride concentration in overlying water was ranged within $1.6-1.9 \times 10^4$ mg/L (Figure 4-1b). Thin layer caps had an unobvious influence on chloride ions throughout the study.

Total Fe concentration ranged between 0.3 and 0.4 mg/L (Figure 4-1c). Total Fe was found to have a slightly positively correlation ($R^2 = 0.3393$; $0.1207 \le R^2 \le 0.5579$

under 95% confidence level) with sulfate concentrations (Figure S4-9).

Both the intermittent turbation test (the vibration system was stopped during day 20-31) and the sediment sampling events (non-purposed incident) have caused impact to Fe escape into the overlying water. Two concentration peaks of total Fe were observed in the AC + montmorillonite caps and the control experiment after the intermittent turbation test and the sediment sampling event. Capping with the AC + bentonite and the AC +kaolin showed little response to these two events and resulted in low total Fe concentration throughout the study.

The results of sulfate and total Fe indicate that the thin layer caps could provide a barrier to decrease sediment-to-water flux of these elements. Capping with the AC + bentonite and the AC + kaolin was found to decrease sediment-to-water flux of sulfate (35.0-75.0% and 5.9-37.5% reduction, respectively) and total Fe (71.4-96.7% and 28.6-93.3% reduction, respectively); while capping with the AC + montmorillonite showed profound escape of sulfate and total Fe comparable to the control (0.0-11.1% and -64.3-28.6% reduction, respectively).

4.3.3 Reduction of Aqueous THg and MeHg by Thin Layer Cap

Similar to the aqueous sulfate and total Fe, the application of thin layer caps with

the AC + bentonite and the AC + kaolin successfully inhibited Hg sediment-to-water flux under the turbation condition (Figure 4-2, Table S4-6). However, the AC + montmorillonite cap showed less effectiveness in Hg reduction, also resulted in several Hg escape incidents likely referring to two sediment turbation events. In general, THg reduction by the AC + bentonite and the AC + kaolin reached 40.1–95.8% and 34.9-94.3%, respectively in comparison to that shown in the control (Figure S4-10a); while the AC + montmorillonite showed fluctuated THg reduction (-109.4–79.2%) and was highly dependent on the turbation events.

THg reduction in the overlying water was observed after all three caps were applied. This result may be due to the high Hg sorption of AC or instant barrier blocking of the Hg flux by clays. During the intermittent test, THg reached the smallest concentration in all cells due to the less Hg resuspension without turbation. After the intermittent test, THg in all cells raised dramatically likely due to the artificial turbation. During this phase (day 34–54), the AC + bentonite (27.3–179.4 ng/L) and the AC + kaolin (46.1–130.9 ng/L) showed better resistance for THg resuspension into the overlying water as compared to the AC + montmorillonite (206.3–348.3 ng/L) and the control (198.4–415.7 ng/L). After day 54, an unintentional sediment sampling event partially disturbed the surface sediment (1–3 cm), causing a dramatic THg escape in the control and the AC + montmorillonite.

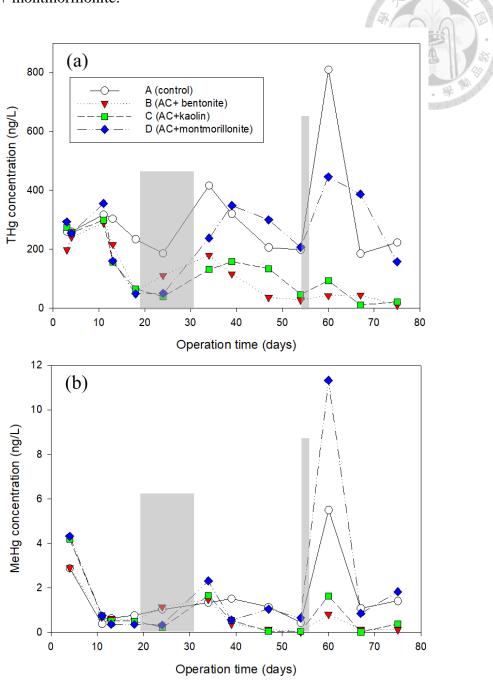


Figure 4-2. (a) THg and (b) MeHg concentration in the overlying water of four cells of the microcosm. The gray bar between day 20 and 30 represents intermittent turbation test; the gray bar at day 54 represents the sediment sampling event.

MeHg in the overlying water showed a similar pattern to THg (Figure 4-2, Table

4-S6). The AC + bentonite and the AC + kaolin showed smaller MeHg concentration (0.01-1.48 ng/L and 0.01-1.65 ng/L, respectively) as compared to the AC + montmorillonite and the control (0.43-5.50 ng/L and 0.32-11.33 ng/L, respectively). Although the MeHg reduction by capping was not obvious in the earlier phase (< 34 d), probably due to the complex microbial community alteration after the thin layer capping was applied, after day 34, both the AC + bentonite and the AC + kaolin caps were highly efficient in MeHg reduction (by 75.89–98.06% and 64.7–98.9%, respectively) in comparison to the control (Figure S4-10b). In contrast, MeHg reduction by the AC + montmorillonite showed contradicted results (-106.1–63.4%). A breakthrough of MeHg (11.33 ng/L) was observed after the unintentional sediment sampling events (day 60).

Based on these experimental observations, the levels of sulfate, total Fe, THg, and MeHg in overlying water were concluded to be highly dependent on the sediment-to-water flux altered by the quality of the caps. The relationships of THg/MeHg to sulfate and total Fe were carried out in Figures S4-11 and S4-12. THg was found to be mildly strong positive correlated to sulfate ($R^2 = 0.3415$; $0.1229 \le R^2 \le 0.5601$ under 95% confidence level) and to total Fe ($R^2 = 0.3653$; $0.1474 \le R^2 \le 0.5832$ under 95% confidence level). In comparison, the correlation for MeHg to sulfate and to total Fe

was less correlated. This may be because of that the origin of MeHg is by biosynthesized and thus can be altered may much more complex mechanisms rather than direct Hg release. THg also showed mildly positive correlated ($R^2 = 0.2882$; $0.0712 \le R^2 \le 0.5052$ under 95% confidence level) with MeHg (approximately 0.21% of THg) (Figure S4-13). The connection between biogeochemical factors (e.g. sulfate and Fe) toward Hg fate was exceedingly complex and has drawn much attention to scientists. Under sulfate-limiting conditions (<20–30 mg/L) [133, 134], sulfate was considered favorable to Hg methylation process by facilitating microbial processes. However, greater sulfate concentration may result in inhibiting methylation by sulfide toxicity toward methylators or reducing more bioavailable HgS₀ form [135]. The high sulfate concentration $(2.0-2.5\times10^3 \text{ mg/L})$ obtained in this study may partly explain the MeHg/THg ratio (0.21%) at the low end as compared to other salt marsh or sediments [136].

4.3.4 ORP, THg, and MeHg in Sediment

All thin layer caps showed the reduction of ORP in sediment in the 75-days trial (Figure 4-3). Without caps, the ORP of sediment ranged -148--176 mV. As anticipated, all capping showed a decrease in ORP [137, 138]. Capping with the AC + bentonite and the AC + kaolin showed the greatest reduction to -250.5 - -257.5 mV and -257.2-

-265.4 mV, respectively. Capping with the AC + montmorillonite was observed to have a smaller reduction in ORP (-177.4– -226.1 mV) as compared to the other two caps scenarios, probably due to lacking stability.

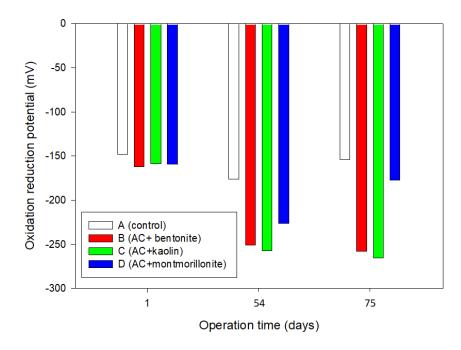


Figure 4-3. The ORP in sediment of the four cells of the microcosm. The ORP was measured within 1–3 cm depth.

The sediment THg (1-3 cm) in all cells was found to decrease from original concentration (76.0 mg/kg) to 58.6–64.52 mg/kg (with caps) and 66.46±2.38 mg/kg (control) (Figure 4-4). Since the microcosm is an open-channel system, it was reasonable that Hg escape may stem from the THg gradient from sediment to open air by diffusion or Hg reduction into the gaseous phase (as Hg⁰). After capping, all capping groups had slightly smaller sediment THg (46.6–66.4 mg/kg) as compared to control (66.5–67.0 mg/kg), likely due to the sorption of Hg by caps, or the caps served as

barriers preventing from Hg-containing particulates to re-supply to the sediment (1-3 cm).

Sediment MeHg remained steady in the control $(2.70-3.34 \ \mu g/kg)$ but showed fluctuation in different caps (Figure 4-4). In the AC + bentonite, MeHg in sediment gradually decreased from 3.10 ± 0.11 to $1.94\pm0.74 \ \mu g/kg$. However, the AC + kaolin and the AC + montmorillonite showed a decrease in sediment MeHg in day 54, but increase to up to 5.391 ± 0.09 and $4.60\pm0.32 \ \mu g/kg$ in day 75, respectively. The decrease in MeHg can be explained by microbial communities shift after the capping events. The other reason may be because the AC application to the sediment reduced MeHg production potential, which was obtained by other microcosms studies [65, 66]. The lateral increase (day 75) of sediment MeHg may be because of the ORP decrease due to capping [137, 138], facilitating the occupation of anaerobic methylators in sediments. The fluctuation of sediment MeHg under thin layer caps may be governed by complex mechanisms and can thus be variable or not altogether predictable.

A significant breakthrough of Hg in the overlying water occurred for a labile cap, such as the AC + montmorillonite, after sediment sample events (which disturbed the sediment in depth of 1-3 cm). However, for the more stable caps (i.e., AC + bentonite and AC + kaolin), the stability of caps enhanced the resistance for Hg breakthrough to the overlying water. The reason for greater Hg escape in the control and the AC + montmorillonite may be due to the destruction of the anoxic zone beneath sediment by turbation, resulting in releasing MeHg, which was stably stored under the caps [138] to the overlying water. On the other hand, the AC + bentonite and the AC + kaolin were more capable of recovering the destruction zone by the immediate settling clay.

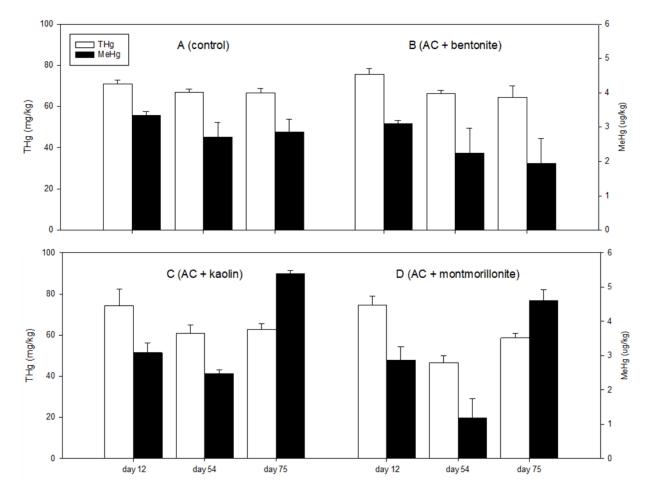


Figure 4-4. THg and MeHg in the sediment (1-3 cm depth) of the four cells of the

microcosm (n = 3).

4.3.5 The Stability of Thin Layer Caps during Turbation

A more explicit scope has been revealed that the stability of thin layer caps significantly alters multiple elements (sulfate, total Fe, THg, and MeHg) from escaping to the overlying water under turbation environment. Both the AC + bentonite and the AC + kaolin thin layer caps successfully immobilized THg and MeHg as well as sulfate and total Fe from escaping even within horizontal flow and turbation. A labile cap, which is the AC + montmorillonite, was unable to stabilize in the surface of sediment and resulted in dramatic Hg escape when encountered turbation.

4.4 Summaries

The results of this study may provide an explanation for previous studies or new perspectives for direction to future capping technologies. Previous studies have shown contradicting results, as some studies suggested that turbation promotes contaminant sequestration in sediment by promoting mixing process of the surface sediment [124], but some also suggested the turbation may increase sediment-to-water contaminant flux [34, 118]. Some studies focused on the porewater Hg reduction while BC materials were applied to the Hg-contaminated sediment [65, 66, 68]. However, the transport of Hg did not always rely on porewater diffusion but instead on fine particle resuspension [15, 16, 93]. As the transport of Hg on the fine particles was discovered in Penobscot

[15, 16], the risk exists if the biochar amendment increases solid-phase MeHg, further escapes to surface water with tidal movements. It is essential to note that with unstable caps, a high concentration of MeHg breakthrough from contaminated sediment can be expected in the occurrence of turbation in a given depth. Concerning using thin layer caps as the solution for Hg-contaminated sites, the stability of thin layer caps is crucial and great attention should be paid to.

4.5 Supporting Information

Table S4-1. Properties for ANS sediment.

| | Water | pН | CEC | Organic | Sand | Silt | Clay | THg |
|----------|-----------|-----------|------------|-----------|----------|----------|----------|------------|
| | content | pm | CLC | content | Sand | Siit | Clay | |
| | (wt%) | (-) | (cmol+/kg) | (wt%) | (wt%) | (wt%) | (wt%) | (mg/kg) |
| ANS | 2.33±0.01 | 7.52±0.03 | 3.3±0.2 | 0.80±0.65 | 71.4±2.9 | 14.3±0.0 | 14.3±2.9 | 76.0±2.593 |
| sediment | 2.35±0.01 | 1.52±0.05 | 5.5±0.2 | 0.00±0.03 | /1.+_2.7 | 14.5±0.0 | 17.322.7 | 70.0±2.373 |

| Table S4-2. Prop | able S4-2. Properties for ANS surface water. | | | | | | | | | | | |
|------------------|--|-------|-----------|------------|------------|------------------------|-----------|-----------|--|--|--|--|
| | Electrical | pH | | Sulfide | Sulfate | Chloride | THg | MeHg | | | | |
| | (µS/cm) | (-) | (mg/L) | (mg/L) | (100 mg/L) | (10 ³ mg/L) | (ng/L) | (ng/L) | | | | |
| ANS surface | $2.15\pm0.14\times10^{4}$ | 8.342 | ND(<0.05) | ND(<0.05) | 7.5±0.3 | 14.9±0.7 | 143.7±3.4 | ND(<0.02) | | | | |
| water | 2.13_0.1 10 | 0.012 | | 112(10103) | 1.0_0.0 | 11.7_0.7 | 110.7_0.1 | | | | | |



Table S4-3. Operation record for the microcosm.

| Date | Op. day | Operator | Op. record | Motors malfunction |
|------------------------|------------|----------|--|-----------------------|
| 2018 May 2nd | -98 | Yu Ting | 3.5 kg ANS sediment added, pumps stopped for a night. | - |
| 2018 May 3rd | -97 | Yu Ting | Pumps started, added 200 g rectifier medium to each cell. | - |
| 2018 July 7th | -31 | Yu Ting | First attempt adding vibration system to each cell (5 motors/cell). | - |
| 2018 July 10th | -28 | Yu Ting | Vibration stopped, all motors retrieved. | - |
| 2018 August 8th | 1 | Yu Ting | Second attempt adding vibration system to each cell (5 motors/cell). ORP measured. | A3, C1 |
| 2018 August 10th | 3 | Yu Ting | Overlying water sampled in all cells for measurement. | B1, C4, D3 |
| 2018 August 11th | 4 | Yu Ting | Overlying water sampled in all cells for measurement. | D2 |
| 2018 August 15th | 8 | Yu Ting | Motors replacement (A3, B1, C1,C4, D2, D3). | - |
| 2018 August 18th | 11 | Yu Ting | Overlying water sampled in all cells for measurement. | B2 |
| 2018 August 19th | 12 | Yu Ting | Sediment sampled for each cell. Thin layers caps were added in cell B, C, and D. Pumps and motors stopped overnight. | A1, C3, D1, D2 |
| 2018 August 20th | 13 | Yu Ting | Pumps and motors started for 5 h. Overlying water sampled in all cells for measurement. | A3, B3, C1, C2 |
| 2018 August 21st | 14 | Yu Ting | Accumulate motors replacement in this week (A1,A3, B2, B3, C1,C2, C3, D1, D2). | - |
| 2018 August 25th | 18 | Yu Ting | Overlying water sampled in all cells for measurement. | B2, C1 |
| 2018 August 27th | 20 | Yu Ting | All motors stopped for testing the effect of variation of turbation. | - |
| 2018 August 31st | 24 | Yu Ting | Overlying water sampled in all cells for measurement. | - |
| 2018 September 7th | 31 | Yu Ting | All motors started. | - |
| 2018 September 10th | 34 | Yu Ting | Overlying water sampled in all cells for measurement. | A1, A3, B1, C5, D2 |



| 2018 September 12th | 36 Yu Ting | Motors replacement (A1, A3, B1, B2, C1, C5, D2). | - |
|-------------------------------|------------|---|----------------|
| 2018 September 15th | 39 Yu Ting | Overlying water sampled in all cells for measurement. | - |
| 2018 September 20th | 44 Yu Ting | Pump of D cell malfunctioned and replaced. | A3, B2, C2 |
| 2018 September 23rd | 47 Yu Ting | Overlying water sampled in all cells for measurement. | A4, B3, D1, D3 |
| 2018 September 26th | 50 Yu Ting | Motors replacement (A3, A4, B2, B3, B5, C2, D1, D3). | - |
| 2018 September 30th | 54 Yu Ting | Overlying water sampled in all cells for measurement. Sediment sampled for each cell. ORP measured. | A1, A4, B4 |
| 2018 October 2nd | 56 Yu Ting | Motors replacement (A1, A4, B4). | |
| 2018 October 6th | 60 Yu Ting | Overlying water sampled in all cells for measurement. | A3, B3, C3, D1 |
| 2018 October 9th | 63 Yu Ting | Motors replacement (A3, B3, C3, D1). | - |
| 2018 October 13 th | 67 Yu Ting | Overlying water sampled in all cells for measurement. | - |
| 2018 October 18 th | 73 Yu Ting | wire reformed. Motors replacement (B5) | B5 |
| 2018 October 20 th | 75 Yu Ting | Overlying water sampled in all cells for measurement. Sediment sampled for each cell. ORP measured. | - |

Table S4-3 continued.



Table S4-4. Temperature, DO, pH, and EC of the overlying water in the microcosm.

| | Temperature DO | | | | рН | | | | | EC | | | | |
|-----|----------------|------|------|------|------|------|------|------|------|-------|--------|--------|-------|--|
| | (°C) | | (mg | g/L) | | | | | | | (100 µ | ıS/cm) | | |
| Day | | А | В | С | D | А | В | С | D | А | В | С | D | |
| 4 | 26 | 6.01 | 6.09 | 6.26 | 6.37 | 7.77 | 7.78 | 7.73 | 7.77 | 362.0 | 353.0 | 379.0 | 364.0 | |
| 11 | 22 | 6.56 | 6.96 | 6.96 | 6.58 | 7.73 | 8.02 | 8.03 | 8.06 | 391.0 | 278.0 | 306.0 | 306.0 | |
| 13 | 24 | 6.17 | 6.10 | 6.13 | 6.32 | 8.14 | 8.11 | 8.16 | 8.22 | 339.0 | 286.0 | 332.0 | 308.0 | |
| 18 | 25 | 5.86 | 6.19 | 6.17 | 6.22 | 8.18 | 8.21 | 8.25 | 8.22 | 308.0 | 270.0 | 318.0 | 343.0 | |
| 34 | 25 | 6.65 | 6.05 | 5.87 | 6.46 | 8.25 | 8.10 | 8.07 | 8.05 | 332.0 | 222.0 | 291.0 | 312.0 | |
| 39 | 26 | 6.50 | 6.16 | 5.67 | 6.04 | 8.03 | 8.16 | 8.27 | 8.24 | 336.0 | 205.0 | 290.0 | 308.0 | |
| 47 | 26 | 6.50 | 6.08 | 6.07 | 6.04 | 8.04 | 8.15 | 8.06 | 8.23 | 335.0 | 204.0 | 258.0 | 303.0 | |
| 54 | 24 | 6.43 | 6.65 | 6.28 | 6.84 | 8.07 | 8.23 | 8.15 | 8.14 | 323.0 | 208.0 | 274.0 | 309.0 | |
| 60 | 22 | 6.56 | 6.61 | 5.89 | 6.61 | 8.17 | 8.29 | 8.24 | 8.24 | 312.0 | 219.0 | 253.0 | 330.0 | |
| 67 | 22 | 6.69 | 6.86 | 6.69 | 6.60 | 8.29 | 8.35 | 8.20 | 8.22 | 319.0 | 200.0 | 253.0 | 323.0 | |
| 75 | 24 | 6.95 | 5.85 | 6.43 | 6.97 | 8.26 | 8.39 | 8.15 | 8.11 | 310.0 | 222.0 | 259.0 | 328.0 | |



| | | | | | | | | | | | | | | | 7 | AIT | |
|-----|------|-------|-------|------|----|-----------------|------|----|------|-------------|-------|------|--------|------|------|------|--|
| | Cl- | | | | | S ²⁻ | | | | SO_4^{2-} | | | Fe ion | | | | |
| | | (1000 | mg/L) | | | (mg | g/L) | | | (100 1 | mg/L) | | | (mg | g/L) | | |
| Day | А | В | С | D | А | В | С | D | А | В | С | D | А | В | С | D | |
| 4 | 18.0 | 17.8 | 18.0 | 17.7 | ND | ND | ND | ND | 25.0 | 24.0 | 22.0 | 21.0 | 0.42 | 0.33 | 0.30 | 0.32 | |
| 11 | 16.3 | 16.3 | 17.0 | 17.0 | ND | ND | ND | ND | 28.0 | 26.0 | 21.0 | 24.0 | 0.37 | 0.43 | 0.36 | 0.36 | |
| 13 | 18.7 | 17.8 | 18.6 | 18.1 | ND | ND | ND | ND | 30.0 | 25.0 | 27.0 | 27.0 | 0.37 | 0.17 | 0.22 | 0.20 | |
| 18 | 18.4 | 17.7 | 17.8 | 17.8 | ND | ND | ND | ND | 20.0 | 13.0 | 18.0 | 18.0 | 0.4 | 0.07 | 0.39 | 0.29 | |
| 24 | 17.6 | 16.8 | 17.4 | 17.9 | ND | ND | ND | ND | 17.0 | 11.0 | 16.0 | 18.0 | 0.33 | 0.07 | 0.14 | 0.44 | |
| 34 | 17.2 | 17.4 | 17.5 | 18.7 | ND | ND | ND | ND | 19.0 | 9.0 | 14.0 | 15.0 | 0.50 | 0.03 | 0.08 | 0.57 | |
| 39 | 17.1 | 17.3 | 18.5 | 18.9 | ND | ND | ND | ND | 17.0 | 6.0 | 13.0 | 16.0 | 0.60 | 0.02 | 0.04 | 0.44 | |
| 47 | 17.1 | 15.9 | 15.9 | 16.2 | ND | ND | ND | ND | 19.0 | 7.0 | 11.0 | 13.0 | 0.28 | 0.09 | 0.04 | 0.46 | |
| 54 | 18.1 | 17.3 | 17.8 | 18.3 | ND | ND | ND | ND | 18.0 | 8.0 | 13.0 | 16.0 | 0.14 | 0.04 | 0.04 | 0.10 | |
| 60 | 16.3 | 16.0 | 15.5 | 15.8 | ND | ND | ND | ND | 15.0 | 7.0 | 12.0 | 15.0 | 0.56 | 0.05 | 0.05 | 0.75 | |
| 67 | 16.7 | 14.3 | 14.8 | 16.4 | ND | ND | ND | ND | 16.0 | 7.0 | 11.0 | 16.0 | 0.04 | 0.00 | 0.00 | 0.05 | |
| 75 | 18.8 | 17.3 | 17.3 | 18.2 | ND | ND | ND | ND | 16.0 | 4.0 | 10.0 | 15.0 | 0.07 | 0.04 | 0.05 | 0.05 | |

Table S4-5. chloride, sulfate and total Fe contents of the overlying water in the microcosm.



| | | Tota | MeHg | | | | | | | |
|-----|--------|--------|--------|--------|------|------|------|-------|--|--|
| | | (ng | y/L) | (ng/L) | | | | | | |
| Day | А | В | С | D | А | В | С | D | | |
| 3 | 260.18 | 197.40 | 274.70 | 292.78 | - | - | - | - | | |
| 4 | 260.27 | 240.68 | 256.61 | 254.13 | 2.88 | 2.89 | 4.19 | 4.32 | | |
| 11 | 317.94 | 289.08 | 298.13 | 355.17 | 0.38 | 0.69 | 0.73 | 0.74 | | |
| 13 | 303.84 | 216.38 | 156.28 | 159.63 | 0.62 | 0.63 | 0.52 | 0.35 | | |
| 18 | 234.41 | 58.22 | 64.95 | 48.62 | 0.76 | 0.53 | 0.49 | 0.35 | | |
| 24 | 185.77 | 110.69 | 38.59 | 50.02 | 1.03 | 1.14 | 0.21 | 0.32 | | |
| 34 | 415.65 | 179.36 | 130.88 | 237.75 | 1.33 | 1.48 | 1.65 | 2.31 | | |
| 39 | 320.25 | 116.10 | 157.50 | 348.30 | 1.50 | 0.36 | 0.53 | 0.55 | | |
| 47 | 205.86 | 36.22 | 134.11 | 300.00 | 1.14 | 0.14 | 0.04 | 1.03 | | |
| 54 | 198.43 | 27.32 | 46.11 | 206.32 | 0.43 | 0.01 | 0.04 | 0.64 | | |
| 60 | 809.77 | 42.33 | 92.90 | 445.55 | 5.50 | 0.80 | 1.63 | 11.33 | | |
| 67 | 184.83 | 44.06 | 10.62 | 387.01 | 1.08 | 0.13 | 0.01 | 0.84 | | |
| 75 | 223.46 | 9.35 | 20.11 | 157.56 | 1.41 | 0.11 | 0.37 | 1.82 | | |

Table S4-6. THg and MeHg of the overlying water in the microcosm.



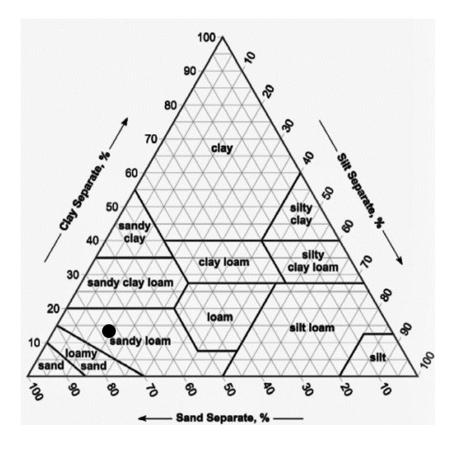


Figure S4-1. The texture of ANS sediment.

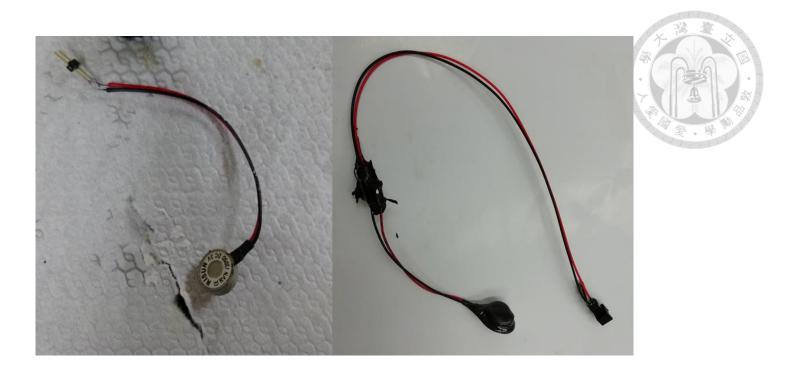


Figure S4-2. Photo diagrams for commercial motors (RISUN PVN 1305D 3V) before (left) and after (right) coated with layers of Hg-free epoxy resin and plastic steels.

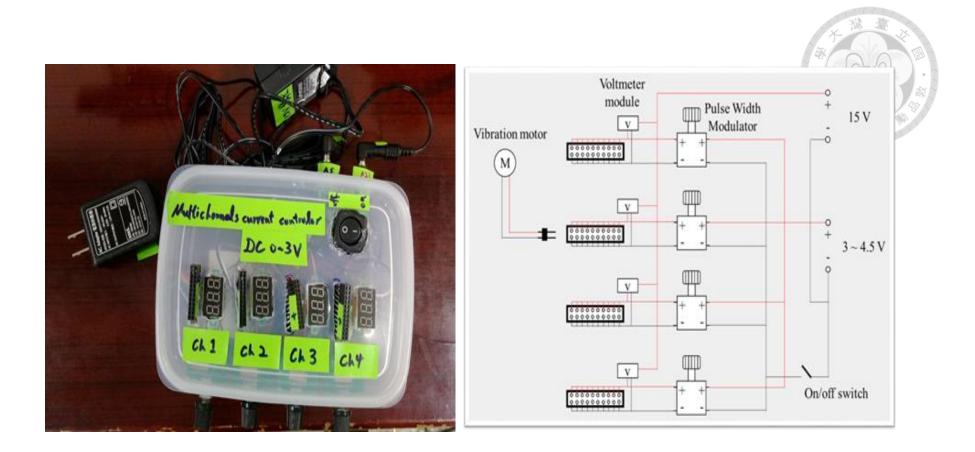


Figure S4-3. Photo diagram (left) and circuit diagram (right) of the lab-made current controller.





Figure S4-4. Photo diagram of the whole microcosm. The yellow stars represent the location of the motors; the blue arrow represents the sampling point for overlying water and the beneath sediment.

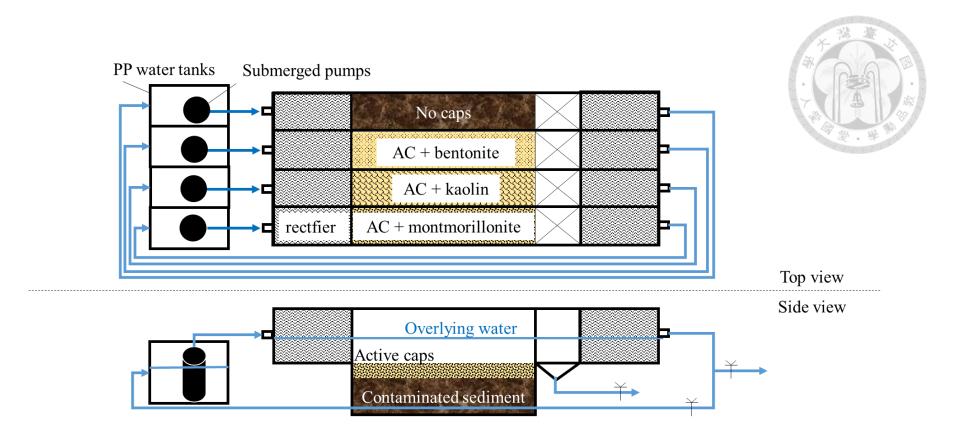


Figure S4-5. Scheme diagram of the microcosm construction.



Figure S4-6. Photo diagrams for the start-up of the microcosm, including the pressure test (up), sediment incubation (middle; day -98) and rectifier added (down; day -97).

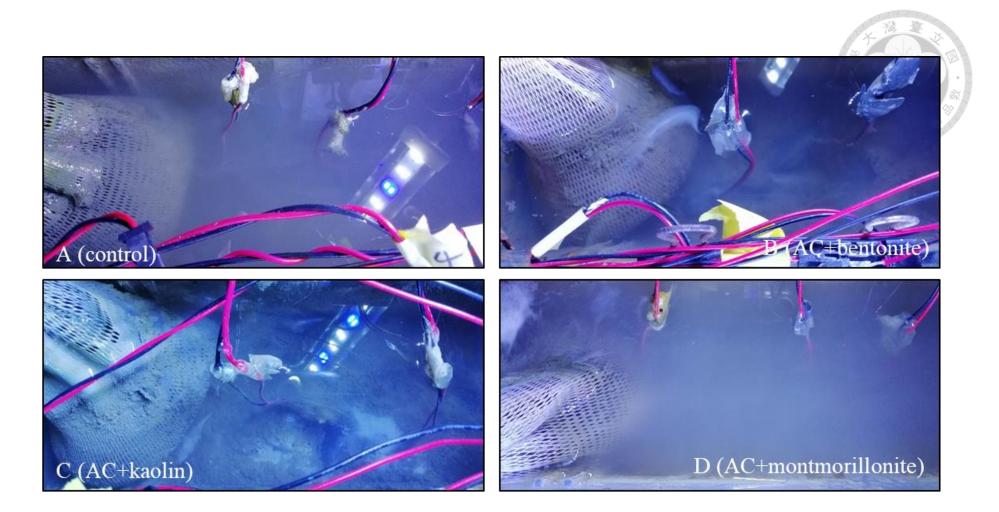


Figure S4-7. Top view of cell A (control), cell B (AC + bentonite), cell C (AC + kaolin) and cell D (AC + montmorillonite); the photographs were taken at day 70.

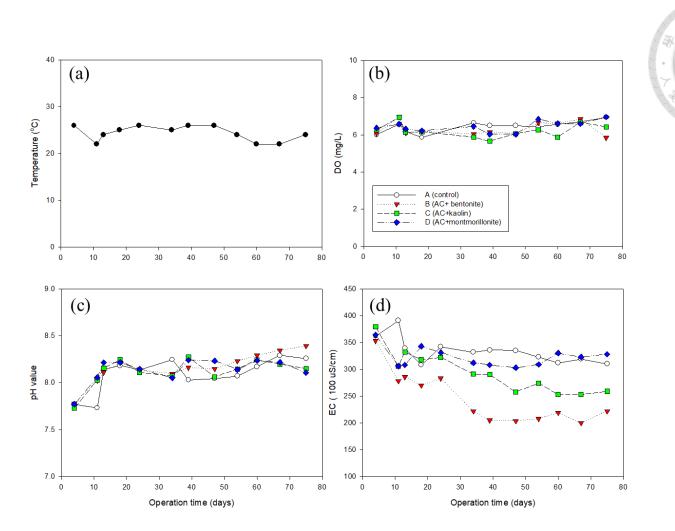


Figure S4-8. (a) Temperature, (b) DO, (c) pH, and (d) EC of the overlying water in the microcosm.

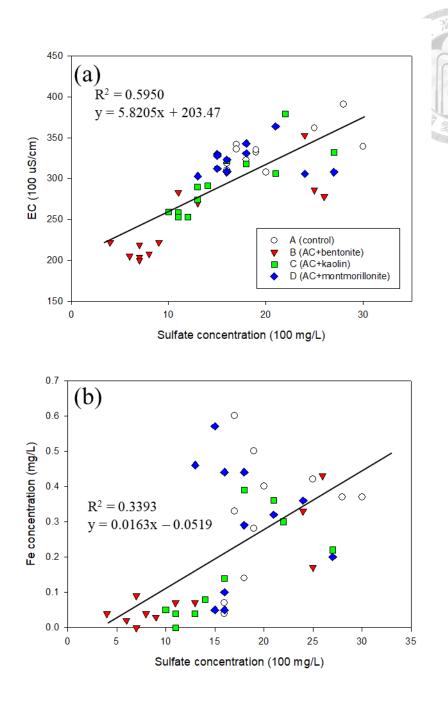


Figure S4-9. Correlation of sulfate to (a) EC (n = 46) and (b) total Fe (n = 43). An extreme data point of day 60 was removed from the plot.

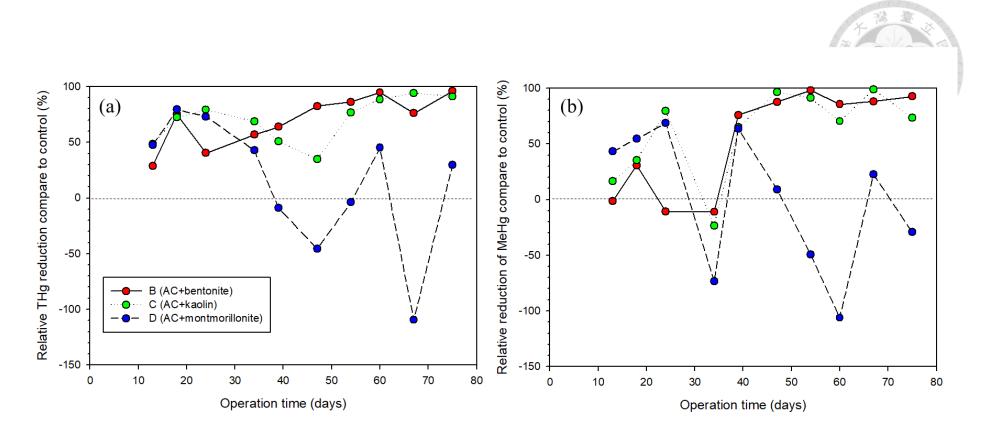


Figure S4-10. (a) THg reduction and (b) MeHg reduction efficiency of thin layer caps in comparison to control.

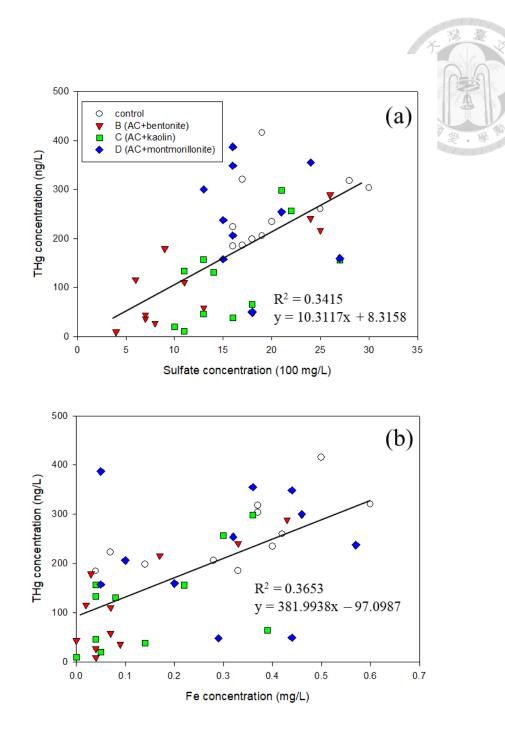


Figure S4-11. Correlation of THg to (a) sulfate and (b) total Fe. Extreme data points of day 60 were removed. (n = 43)

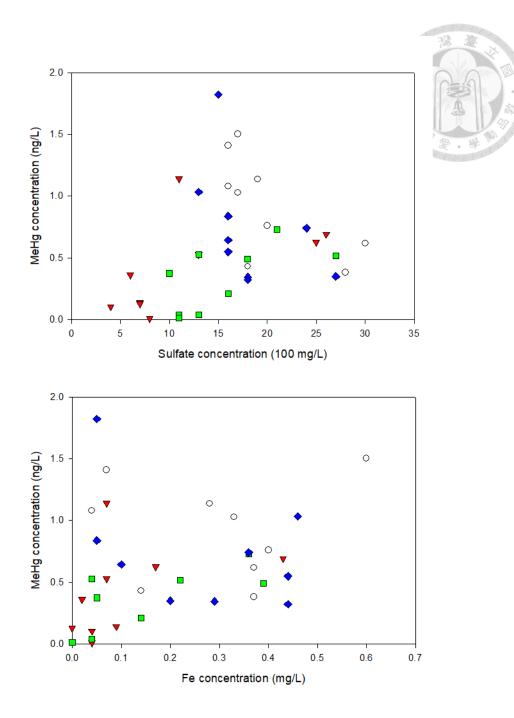


Figure S4-12. Correlation of MeHg to (a) sulfate and (b) total Fe. Extreme data points of day 34 and day 60 were removed.

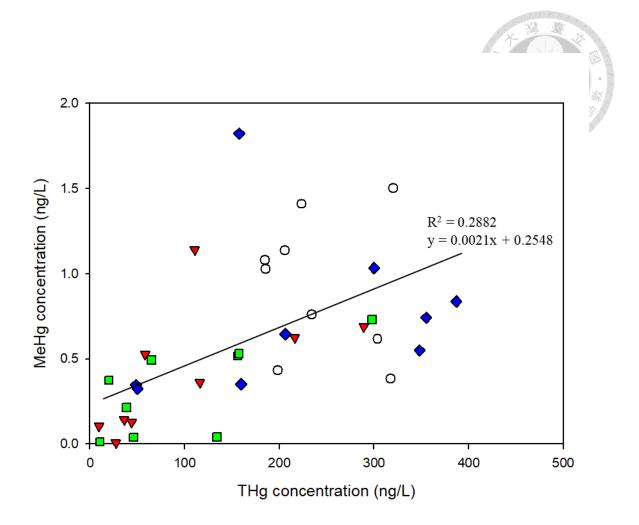


Figure S4-13. Correlation of THg to MeHg. An extreme data point of day 60 was removed. (n = 43)

Chapter 5 Conclusions and Suggestions

This thesis tackled two major aspects for thin layer capping to apply on Hgcontaminated sediment by two separate studies. The first study attempted to enhance Hg sorption ability by modifying sulfur functional groups on AC; the second study evaluated the stability of caps during turbation events.

During the first study, we observed a successful enhancement of Hg sorption affinity by sulfurized raw AC material in aqueous adsorption tests, which is consistent with some past studies proceeded in similar conditions. However, these studies did not account for the effect of sediment environment which may contain complex biogeochemical factors (e.g. DOM) that alter the fate of Hg. We observed a reversal results as SAC had lower Hg sorption compare to AC in the sediment competition tests. We thus suspect that the sulfur functional groups on the surface of AC can be released and mobilized Hg in the aqueous phase in DOM-rich environments, as described in section 3.3.3. In further inference, it suggests that the sulfurized AC may not enhance Hg sorption during thin layer capping remedy but rather the opposite. However, we also do not suggest that all sorbents with sulfur functional groups may be useless in terms of in-situ sediment remediation, as sulfur functional groups present in various forms and can be varied in results. The results of the microcosm study also differ from sediment adsorption tests as all caps performed with similar Hg reduction efficiency. Further studies to find out the relation between sulfurized sorbents and DOM can be crucial in this technology.

The second study provided some pioneer findings of the relations between the stability of thin layer caps and sediment turbation, which were often questioned by the scientific community. Our results suggested caps with AC + kaolin and AC + bentonite

can be stable and were efficient in reducing both THg and MeHg in overlying water and observed with better resistance during occasional turbation events. On the other hands, AC + montmorillonite showed poor Hg reduction efficiency in general and Hg breakthrough in occasional turbation events. Our results suggested that the successfulness of this remedy can be altered not only by the main sorbents but also anchoring materials (e.g. clay minerals). The previous studies related in this field have focused on the porewater Hg as the parameter for the effectiveness of the sorption tests. However, transportation of Hg through sediment particles was proposed and observed in recent studies, which is also consistent with our observation. Also, the different levels of Hg breakthrough may not necessary alters by the different Hg methylation activities, as observed in our results. Thus, it requires further studies to explore the relations between sediment turbation and the Hg reduction efficiency of thin layer caps.

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