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#### 碩士論文

Graduate Institute of Applied Physics College of Science National Taiwan University

Master Thesis

使用熱輔助佔據密度泛函理論對融合薁並苯之電子性 質的理論研究

Theoretical studies of electronic properties of fused azulene-acene

using thermally-assisted-occupation density functional theory

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#### 摘要



本論文使用熱輔助佔據密度泛函理論(thermally-assisted-occupation density functional theory, TAO-DFT) 在局部密度近似(local density approximation, LDA) 下研究融合奠並苯(fused azulene-acene)系統的電子性質,並與其同分異構物並 苯(acenes)比較。若使用孔沈密度泛函理論(Kohn-Sham density functional theory, KS-DFT)計算融合奠並苯系統,會產生因其強關聯(strongly correlated)特性而 發生的靜態關聯誤差(static correlation error, SCE),得到物理上不正確的三重態基 態(triplet ground state)。另一方面,孔沈密度泛函理論的計算過程中容易收斂到 局域最小值,因此必須用大量初始條件和算法才能得到全域最小值,相較之下熱 輔助佔據密度泛函理論能有效收斂到絕對最小值且修正靜態關聯誤差,同樣的計 算資源下更有效率,因此本篇論文使用熱輔助佔據密度泛函理論來研究融合奠並 苯系統的電子性質。

在短鏈 (n<8) 融合奠並苯系統中使用基於孔沈密度泛函的混成泛函 B3LYP 得到負的單重態三重態能量差 (Singlet-Triplet gap),而使用熱輔助佔據 B3LYP 的 計算結果皆為正,也就是單重態基態。在局部密度近似下,長鏈 (n<75)的融合奠 並苯的單重態三重態能量差皆小於並苯的能量差,得知兩端融合七五環可以將其 降低,且減少幅度隨著長度增加而減少。從對稱馮諾伊曼熵 (symmetrized von Neumann entropy) 和軌域佔據數可以得知融合奠並苯的多重參考性 (multireference),且從對稱馮諾伊曼熵對於鏈長的關係發現融合奠並苯與並苯斜率相同 向上平移,發現融合奠並苯的軌域佔據數結構與並苯的類似。

關鍵字:融合薁並苯、並苯、熱輔助佔據密度泛函理論、強關聯系統

iii

### Abstract



In this thesis, we investigate the electronic properties of fused azulene-acene system using thermally-assisted-occupation density functional theory (TAO-DFT) in local density approximation (LDA) and compare to the properties of its isomer, acenes. If we use Kohn-Sham density functional theory (KS-DFT) to calculate, we get unphysical triplet ground state because of static correlation error (SCE) causing by the strong correlated (SC) character of fused azulene-acene. On the other hand, the energy usually truncate to local minimum during the iterating process of KS-DFT, and thus it needs lots of initial guess and algorithm to find the global minimum. TAO-DFT can effectively truncate to global minimum and correct SCE under the same computational resource, therefore is used to calculate the properties of fuse azulene-acene.

Negative singlet-triplet energy gap is obtained using hybrid functional B3LYP based on KS-DFT for fused azulene-acene in short length (n<8). The result is positive, namely siglet ground state, using TAO-B3LYP. In LDA, singlet-triplet gaps of fused azulene-acene are all lower than ones of acenes. We can know that fusing the 7, 5 rings will lower ST gap, and the degree of reduction decrease as the length increase. Symmetrized von Neumann entropy and orbital occupation numbers show the multireference character of fused azulene-acene. The slope of fused azulene-acene of symmetrized von Neumann entropy to length is the same as one of acenes and translate upward, which indicates fused azulene-acene has similar structure of orbital occupation numbers to acenes.

Keywords: fused azulene-acene, acenes, thermally-assisted-occupation density functional theory, strong correlated system

iv

### Contents



| 致謝ii  |
|---|
| 摘要iii   |
| Abstract iv   |
| Contentsv   |
| List of Figures vii   |
| List of Tables xiii   |
| Chapter 1 Introduction                                      |
| Chapter 2 Theoretical background                            |
| 2.1 Density functional theory                               |
| 2.2 Hohenberg-Kohn theorems                                 |
| 2.3 Kohn-Sham method 10                                     |
| 2.4 Thermally-Assisted-Occupation density functional theory |
| 2.5 Computational Details 17                                |
| Chapter 3 Results   |
| Chapter A. Conculsion 35                                    |

| Chapter 5    | Reference   | 36                   |
|--------------|---|----------------------|
| empter e     |   |                      |
| Appendix A   | : Active orbital occupation numbers for the lowes | st singlet states of |
| fused azuler | ne-acene  |                      |

## **List of Figures**



| 1.1: The structures of (a) n-acenes, (b) azulene and (c) fuse azulene-acene  |
|--|
| 3.1: Four kinds of singlet-triplet energy gaps of fused-azulene-acene, calculated by B3LYP and TAO-B3LYP ( $\theta = 17.4$ mHartree)/6-31G* and reference data [12]  |
| 3.2: Singlet-triplet energy gap of acenes and fused azulene-acenes calculated by TAO-LDA ( $\theta = 7 \text{ mHartree}$ )/6-31G* and TAO-B3LYP ( $\theta = 17.4 \text{ mHartree}$ )/6-31G*  |
| 3.3: Singlet-triplet energy gap of fused azulene-acenes for n from 3 to 46 calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G* and for n from 3 to 75 calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G                             |
| 3.4: Singlet-triplet energy gap for the longer acenes [13] and fused azulene-acenes calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G   |
| 3.5: Active orbital occupation numbers (HOMO-13,, HOMO-1, HOMO, LUMO, LUMO-1,, and LUMO-13) as a function of the fused azulene-acene length calculated using spin-restricted TAO-LDA ( $\theta = 7$ mHartree)/6-31G                      |
| 3.6: Symmetrized von Neumann entropy for the lowest singlet state of fused azulene-acenes and acenes calculated using spin-restricted TAO-LDA ( $\theta = 7$ mHartree)/6-31G29   |
| 3.7: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=3) with their occupation number 1.8157 and 0.1841   |
| 3.8: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene ( $n=4$ ) with their occupation number 1.3877 and 0.6119   |
| 3.9: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene ( $n=5$ ) with their occupation number 1.1038 and 0.8961   |
| 3.10: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=6) with their occupation number 1.0707 and 0.9301  |
| 3.11: Differences between STgap of n-acenes [13] and fused azulene-acene and dipole moment difference between single and triplet state of fused azulene-acene calculating using spin-unrestricted TAO-LDA ( $\theta = 7$ mHartree)/6-31G |

| B.1: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
|--|
| azulene-acene (n=7) with their occupation number 1.1880 and 0.8147                             |
| B.2: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=8) with their occupation number 1.2742 and 0.7320                             |
| B.3: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=9) with their occupation number 1.3406 and 0.6694                             |
| B.4: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=10) with their occupation number 1.3927 and 0.6203                            |
| B.5: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=11) with their occupation number 1.4323 and 0.5825                            |
| B.6: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=12) with their occupation number $1.4628$ and $0.5529$                        |
| B.7: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=13) with their occupation number 1.4257 and 0.5668                            |
| B.8: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=14) with their occupation number $1.3102$ and $0.6857$                        |
| B.9: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused  |
| azulene-acene (n=15) with their occupation number 1.2068 and 0.7927                            |
| B.10: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused |
| azulene-acene (n=16) with their occupation number 1.1160 and 0.8871                            |
| B.11: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused |
| azulene-acene (n=17) with their occupation number $1.0372$ and $0.9693$                        |
| B.12: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused |
| azulene-acene (n=18) with their occupation number 1.0405 and 0.9688                            |
| B.13: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused    |
| azulene-acene (n=19) with their occupation number 1.1018 and 0.9099                            |
| B.14: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused    |
| azulene-acene (n=20) with their occupation number 1.1547 and 0.8589                            |

| B.29: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
|---|
| azulene-acene (n=35) with their occupation number 1.2038 and 0.8138                         |
| B.30: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=36) with their occupation number 1.1789 and 0.8195                         |
| B.31: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n= $37$ ) with their occupation number 1.1394 and 0.8614                     |
| B.32: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=38) with their occupation number 1.1021 and 0.9008                         |
| B.33: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=39) with their occupation number $1.0669$ and $0.9380$                     |
| B.34: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=40) with their occupation number 1.0339 and 0.9730                         |
|   |
| B.35: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=41) with their occupation number $1.0059$ and $1.0027$                     |
| B.36: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=42) with their occupation number $1.0367$ and $0.9736$                     |
| B.37: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=43) with their occupation number 1.0657 and 0.9462                         |
|   |
| B.38: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=44) with their occupation number $1.0928$ and $0.9204$                     |
| B.39: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=45) with their occupation number 1.1182 and 0.8963                         |
| B.40: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=46) with their occupation number 1.1420 and 0.8737                         |
|   |
| B.41: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=47) with their occupation number $1.1586$ and $0.8523$                     |
| B.42: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
| azulene-acene (n=48) with their occupation number 1.1286 and 0.8725                         |

| B.43: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
|---|
| azulene-acene (n=49) with their occupation number 1.0998 and 0.9031                         |

游臺

| B.57: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused |
|---|
| azulene-acene (n=63) with their occupation number 1.0331 and 0.9740                         |

游臺

## **List of Tables**



| 3.1: The unrestricted singlet (US), unrestricted triplet (UT), restricted singlet (RS) and restricted triplet (RT) state energy of fused-azulene-acene calculated by B3L VP/6-31G* are given in |
|---|
| Hartrees. The four kind of singlet-triplet energy gaps are in kcal/mol  |
| 3.2: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fused-azulene-acene  |
| calculated by IAO-LDA ( $\theta = 7$ mHartree)/6-31G* are given in Hartrees. The S1 gaps are given in kcal/mol  |
| 3.3: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fused-azulene-acene  |
| calculated by TAO-B3LYP ( $\theta = 17.4$ mHartree)/6-31G* are given in Hartrees. The ST gaps are given in kcal/mol. The restricted singlet (RS) state energy and the energy difference between |
| RS and US (RS-US) are also listed in Hartrees in comparison   |
| 3.4: The unrestricted singlet (US) and unrestricted triplet (UT) energy of linear acenes  |
| calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G* are given in Hartrees. The ST gaps are given in kcal/mol  |
| 3.5: The unrestricted singlet (US) and unrestricted triplet (UT) energy of linear acenes  |
| calculated by TAO-B3LYP ( $\theta = 17.4$ mHartree)/6-31G* are given in Hartrees. The ST gaps   |
| are given in kcal/mol   |
| 3.6: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fused-azulene-acene  |
| and acenes calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G* are given in Hartrees. The ST  |
| gaps of both fused-azulene-acene and acene are given in kcal/mol  |
| 3.7: The unrestricted singlet (US) and the unrestricted triplet (UT) energy of fused azulene-   |
| acenes calculated by TAO-LDA ( $\theta = 7$ mHartree)/6-31G are given in Hartrees. The ST gaps of   |
| fused azulene-acene, acenes [13] and $\Delta$ are given in kcal/mol where $\Delta$ is the difference  |
| between ST gaps of fused azulene-acene and acenes. The dipole moment of US and UT and the   |
| singlet-triplet dipole moment gap are given in debye. The symmetrized von Neumann entropy   |
| of both fused azulene-acene and acenes [13] are given   |
| A: Active orbital occupation numbers (HOMO-13,, HOMO-1, LUMO-1,, LUMO-13) for   |
| the lowest singlet states of fused azulene-acene, calculated by spin-restricted TAO-LDA ( $\theta = 7$  |
| mHartree), using the 6-31G basis set  |

# Chapter 1 Introduction

Semiconductor is a type of materials has an electrical conductivity value falling between that of a conductor and an insulator. The fermi level usually falls between conduction band (CB) and valence band (VB), where charge carriers with enough thermal energy can be excited to CB or VB and diffuse or drift around. This kind of materials has various applications such as electronic, optical or spintronic devices [1][18].

In addition to traditional semiconductor materials, scientists are also interesting in organic electronic materials. One of the fascinating materials is graphene, which is discovered by Andre K. Geim and Konstatin S. Novoselov. Graphene is allotrope of carbon having 2D single layer atoms in honeycomb lattice. It has been researched extensively in decades due to its fascinating properties such as massless relativistic Dirac Fermion, non-zero minimum conductivity, room-temperature integer quantum Hall effect [2][29]. The high electron mobility and long spin lifetimes make graphene possible to be applied in constructing graphene-based electronics and spintronics devices [3]. All these outstanding properties of graphene are due to its two-dimensional monolayer of honeycomb lattice carbon structure, related to their  $\pi$ -conjugated bounding topology. However, gap opening between valence and conduction band makes graphene different from semiconductor silicon [30].

1

Acenes, one dimensional graphene nanoribbons (GNRs), which are formed linearly with benzene rings shown in Figure 1.1(a), have been studied widely owing to their tunable optical gaps. Lattice symmetry breaking and finite size effect produce bandgap in graphene [31][32]. Also, their singlet fission phenomenon has been observed and has several possible usages [4][5]. The electronic structure of acenes has been strongly debated. Some studies predict the existence of triplet ground state or the nonmonotonicity of the decay in the singlet-triplet gap [6]. Due to the  $\pi$ - conjugated system, the static correlated effect is strong in density functional theory (DFT). Kohn-Sham DFT may not finely converge the single point energy to global minimum. High-level ab initio multireference method, such as the density matrix renormalization group (DMRG) algorithm [10], the variational two-electron reduced density matrix (2-RDM) method [11][32], can accurately describe the strong correlated effects. However, these methods can be extremely expensive for long-chained acenes. In contrast, thermally-assistedoccupation density functional theory (TAO-DFT) introduce the Fermi-Dirac distribution to approximate the natural orbital occupation numbers and an additional tunable parameter, a fictitious temperature  $\theta$ . It can effectively reduce the computational cost and find the global minima more accurately.



Figure 1.1: The structures of (a) n-acenes, (b) azulene and (c) fuse azulene-acene

Azulene is isomer of naphthalene, consisting of five and seven membered rings, which is shown in Figure 1.1 (b). Its singlet-triplet (ST) gap is lower than naphthalene

since it is less stable and the dipole moment of singlet state pointing from 7 to 5 membered ring. The reversed polarity of triplet state causing lower ST gap is indicated by Braid's theory of triplet state antiaromaticity [15][16]. Repeated fused azulene shows negative ST gap which means triplet ground state [19]. This observation is different from that of acenes and was predicted from the study using UB3LYP method [20]. The ground state crossover of singlet and triplet may be useful in tuning ST gap of acenes, where the system is designed as fused azulene-acene in Figure 1.1 (c).

Defects, such as line defects or edge defects, often appear during the synthesis of graphene. They can be applied in spin-filter devices [9]. Replacing the two ends of acenes by fused five or seven membered rings can be seen as the edge defects of acenes. Theoretically, the fused azulene-acene have lower ST gap than its isomer of acenes. As the length increase, the effect of the edge defect should be less relevant and the ST gap of the two should converge. Though there is a study of the fused azulene-acene system obtained the results of triplet ground state using UB3LYP geometries and multireference calculations optimizing which against our prediction [12].

In this thesis, we reproduce the result of triplet ground state by using B3LYP to optimize. In comparison, TAO local density approximation (TAO-LDA) and TAO-B3LYP are employing due to its computational efficiency and ability dealing with the strong correlated cases to generate the result similar to the long acenes [8][13][26][34], showing how five and seven membered rings reducing ST gap effectively in short length. In convenient, we define the length of fused azulene-acene with a number n which the molecular formula satisfies  $C_{4n+2}H_{2n+4}$ . Due to the expensive computational costs, we only obtain both spin-restricted and spin-unrestricted B3LYP results from 2 to 8 by assuming lots of initial guesses, and compare the results to triplet ground state references. From 2 to 20, we compute with both spin-unrestricted TAO-LDA and TAO-

3

B3LYP to see the differences between fused azulene-acene and linear acenes. Using TAO-LDA, the length can be calculated up to 75 without initial guesses and thus can be compared to the results of n-acenes, where the singlet-triplet energy gap, orbital occupation numbers, symmetrized von Neumann entropy and dipole moment are included. The electronic properties can provide information for further applications like defect controlling or spintronic devices.

### **Chapter 2**



### **Theoretical background**

#### 2.1 Density functional theory

Density functional theory (DFT) is a popular method widely used in physics, chemistry and materials science in recent years. Using this computational quantum mechanical modelling method, the electronic properties of a many-body systems are allowed to be determined. In many-body problem, the electronic structure is covered by Schrödinger's equation. The solution of this equation is a wave function with 3N spatial coordinates and usually cannot be solved. Due to the complexity solving it, one is interesting in reducing the variables from 3N to only 3 by representing system energies in electric density instead of electric wave functions. The roots of DFT is from the Thomas-Fermi model for the electronic structure of materials. DFT was first given a rigorous proof by Hohenberg and Kohn in 1964 [21]. The original Hohenberg-Kohn theorem describes that both the non-degenerated ground state density and ground state wave function have one to one relation with the system external potential. In 1965, Walter Kohn and Le Jeu Sham followed the Hohenberg-Kohn theorem and developed a practical and computable self-consistent method, which is called Kohn-Sham DFT [22]. In this theory, the many-body problem of interacting electrons in a static external potential is reduced to fictitious non-interacting electrons in an effective potential. Assuming a self-consistent initial condition, the solution of Kohn-Sham equation will converge by iterative process. Kohn-Sham theory puts the concept of DFT into practical calculations to deal with electronic structure, molecules binding energy, materials band

gap and so on.

To get the energy and the 3N-dimensional wave function of an N-electron system, one need to solve the Schrödinger equation

$$\widehat{H}\Psi(\boldsymbol{x}_1,\ldots,\boldsymbol{x}_N,\boldsymbol{R}_1,\ldots,\boldsymbol{R}_N) = E\Psi(\boldsymbol{x}_1,\ldots,\boldsymbol{x}_N,\boldsymbol{R}_1,\ldots,\boldsymbol{R}_N)$$
(2.1.1)

where *E* is the electronic energy,  $\Psi$  is the wave function,  $x_i$  is the coordinates of electron i comprising space coordinates  $r_i$  and spin coordinates  $s_i$  and  $\hat{H}$  is the Hamiltonian operator which includes electronic kinetic energy, potential energy between electrons, nuclear kinetic energy, potential energy between nuclei, and potential energy between nuclei and electrons

$$\widehat{H} = \sum_{i=1}^{N} \left(\frac{1}{2} \nabla_{i}^{2}\right) + \sum_{i=1}^{N} \sum_{i' < i} \frac{1}{|\mathbf{r}_{i} - \mathbf{r}_{i'}|} + \sum_{j=1}^{M} \left(\frac{1}{2m_{j}} \nabla_{j}^{2}\right) + \sum_{j=1}^{M} \sum_{j' < j} \frac{Z_{j} Z_{j'}}{|\mathbf{R}_{j} - \mathbf{R}_{j'}|} - \sum_{i=1}^{N} \sum_{j=1}^{M} \frac{Z_{j}}{|\mathbf{r}_{i} - \mathbf{R}_{j}|}$$

$$(2.1.2)$$

with N, M,  $r_i$ ,  $R_j$ ,  $m_j$ ,  $Z_j$  being the amount of electrons, amount of nuclei, positions of electron i, position of nucleus j, mass of nucleus j and charge number of nucleus j.

In the Born-Oppenheimer nonrelativistic approximation, nuclei are way heavier than electrons and thus considered static. Then the nuclear kinetic energy can be ignored and the potential energy between nucleus can be seen as constant. The Hamiltonian can be simplified as

$$\widehat{H} = \sum_{i=1}^{N} \left(\frac{1}{2} \nabla_{i}^{2}\right) + \sum_{i=1}^{N} v(\mathbf{r}_{i}) + \sum_{i< j}^{N} \frac{1}{\mathbf{r}_{ij}}$$
(2.1.3)

$$=\hat{T}+\hat{V}_{ext}+\hat{V}_{ee} \tag{2.1.4}$$

in which

$$v(r_i) = -\sum_{\alpha} \frac{Z_{\alpha}}{r_{i\alpha}}$$
(2.1.5)

is the external potential acting on electron i due to nuclei of charges  $Z_{\alpha}$ . The wave function can simplified to a 3N variables function  $\Psi(r_1, ..., r_N)$ .

To reach the goal of reducing 3N variables to 3, one wonders if it is possible to represent the system energies terms of electron density. The density function in terms of  $\Psi$  is

$$\rho(\mathbf{r_1}) = N \int \dots \int |\Psi(\mathbf{x_1}, \dots, \mathbf{x_N})| ds_1 d\mathbf{x_2} \dots d\mathbf{x_N}$$
(2.1.6)

which is a simple function of three spatial variables, integrating to the total number of electrons,

$$\int \rho(\mathbf{r})d\mathbf{r} = N \tag{2.1.7}$$

The expectation value of external potential is a function of  $\Psi$ 

$$\langle V_{ext} \rangle = V_{ext}[\Psi] = \langle \Psi | V_{ext} | \Psi \rangle = \int \dots \int \Psi^* V_{ext} \Psi d\mathbf{r_1} \dots d\mathbf{r_N}$$
(2.1.8)

where  $V_{ext}$  is the external potential in (2.1.4). By (2.1.6), (2.1.8) can be simplified as a function of  $\rho$ 

$$V_{ext}[\rho] = \int \rho(r_1) V_{ext}(r_1) dr_1$$
 (2.1.9)

This process shows that we can represent external potential in terms of electron density without assumption. Though  $T[\rho]$  and  $V_{ee}[\rho]$  remain unknown. We can write energy functional as

$$E[\rho] = T[\rho] + V_{ee}[\rho] + \int \rho(\mathbf{r_1}) V_{ext}(\mathbf{r_1}) d\mathbf{r_1}$$
$$= F[\rho] + \int \rho(\mathbf{r_1}) V_{ext}(\mathbf{r_1}) d\mathbf{r_1}$$



where  $F[\rho]$  is the same for all Hamiltonians of N-electron systems.

#### 2.2 Hohenberg-Kohn theorems

For a nondegenerate ground-state N-electron system, the external potential  $V_{ext}$ fixes the Hamiltonian and thus N and  $V_{ext}$  determine ground state energy  $E_0$  and ground state wave function  $\Psi_0$ , and also ground state electron density  $\rho$  by definition. Hohenberg and Kohn in 1964 gave the  $1^{st}$  HK theorem which use electron density as basic variable to determine the external potential instead, showing the one to one relation between ground state electron density and external potential.

Suppose there are two different potential  $V_{ext}{}^{a}(\mathbf{r})$  and  $V_{ext}{}^{b}(\mathbf{r})$  with ground state wave functions  $\Psi^{a}$  and  $\Psi^{b}$  respectively having same density  $\rho$ . We have two Hamiltonians  $H^{a}$ ,  $H^{b}$ ,  $E_{0}{}^{a}$  and  $E_{0}{}^{b}$  accordingly. Taking  $\Psi^{b}$  as a trial function for the  $H^{a}$ , we would have

$$E_0^a < \langle \Psi^b | H^a | \Psi^b \rangle = \langle \Psi^b | H^b | \Psi^b \rangle + \langle \Psi^b | H^a - H^b | \Psi^b \rangle$$
$$= E_0^b + \int \rho(\mathbf{r}) [V_{ext}^a(r) - V_{ext}^b(\mathbf{r})] d\mathbf{r} \qquad (2.2.1)$$

Taking  $\Psi^a$  as a trial function for the  $H^b$ , we have

$$E_0^{\ b} < \langle \Psi^a | H^b | \Psi^a \rangle = \langle \Psi^a | H^a | \Psi^a \rangle + \langle \Psi^a | H^b - H^a | \Psi^a \rangle$$
$$= E_0^{\ a} + \int \rho(\mathbf{r}) [V_{ext}^{\ b}(\mathbf{r}) - V_{ext}^{\ a}(\mathbf{r})] d\mathbf{r} \qquad (2.2.2)$$

Adding (2.2.1) and (2.2.2), we would obtain a contradict equation

$$E_0^{\ a} + E_0^{\ b} < E_0^{\ b} + E_0^{\ a}$$

There cannot be two different external potential  $V_{ext}$  giving the same  $\rho$ . Thus,  $\rho$  determines N and  $V_{ext}$  proved by the 1<sup>st</sup> HK theorem; N and  $V_{ext}$  determines  $\rho$  by solving Schrödinger equation. Density  $\rho$  and external potential  $V_{ext}$  do have one to one relation.

The  $2^{nd}$  HK theorem state that the energy functional gives the minimum energy if and only if the variable density is the ground state density. From the  $1^{st}$  HK theorem, a density  $\tilde{\rho}$  leads to its particular external potential  $\tilde{V}_{ext}$ , Hamiltonian  $\tilde{H}$  and wave function  $\tilde{\Psi}$ . Use a trial density  $\tilde{\rho}$  which is different from ground state density  $\rho_0$  with its own H as the input of energy functional, we have

$$\mathbf{E}[\tilde{\rho}] = \langle \tilde{\Psi} | H | \tilde{\Psi} \rangle > \langle \Psi | H | \Psi \rangle = \mathbf{E}[\rho_0] = E_0 \tag{2.2.4}$$

Assuming differentiability of  $E[\tilde{\rho}]$ , since (2.2.4) indicates that ground state energy satisfies stationary principle, we can apply variational principle with the constraint  $\int \rho(\mathbf{r})d\mathbf{r} - N = 0$ 

$$\delta\{E[\rho] - \mu[\int \rho(r)dr - N]\} = 0$$
 (2.2.5)

which provides the Euler-Lagrange equation

$$\mu = \frac{\delta E[\rho]}{\delta \rho(r)} = V_{ext}(r) + \frac{\delta F[\rho]}{\rho(r)}$$
(2.2.6)

The quantity  $\mu$  is not only a Lagrange multiplier but also chemical potential. The functional F[ $\rho$ ] is universal and independent of the external potential  $V_{ext}$ . We can obtain the energy E[ $\rho$ ] of an individual system if we have the potential associated to the structure and electron density because Hohenberg Kohn theorem gives one to one

(2.2.3)

mapping of the quantities mentioned. Though we cannot solve the exact  $F[\rho]$ , but it is hard to approximate because we simplified the unknown from many-variable wave function  $\Psi$  to a single three-variable function  $\rho$ . To get the minimal energy, what we have to do is searching over all possible density. This is the concept of densityfunctional method for determining the ground-state density and ground-state energy for any system.

#### 2.3 Kohn-Sham method

Kohn and Sham in 1965 developed a method to deal with the kinetic-energy functional  $T[\rho]$  which is less accurate but more practical. The method assumed a non-interacting frame and introduced orbitals. In non-interacting system, electrons do not have repulsion between each other. The Hamiltonian is simplified to

$$H_s = T_s + V_{eff} \tag{2.3.1}$$

Considered orbitals wave function sets, the kinetic energy functional  $T[\rho]$  can be represented as

$$T[\rho] = \sum_{i}^{M} n_{i} \langle \phi_{i} \left| -\frac{1}{2} \nabla^{2} \right| \phi_{i} \rangle$$
(2.3.2)

and the electron density is

$$\rho(\mathbf{r}) = \sum_{i}^{M} n_i \sum_{s} |\phi_i(\mathbf{r}, s)|^2$$
(2.3.3)

where M could be infinite for any interacting system and  $n_i$  is the natural orbital occupation number that  $0 \le n_i \le 1$ . In Kohn-Sham method, the above formulas are simpler, namely

$$T_{s}[\rho] = \sum_{i}^{N} \langle \phi_{i} \left| -\frac{1}{2} \nabla^{2} \right| \phi_{i} \rangle$$



and

$$\rho(\mathbf{r}) = \sum_{i}^{N} \sum_{s} |\phi_{i}(\mathbf{r}, s)|^{2}$$
(2.3.5)

which are fully occupied case of (2.3.2) and (2.3.3) with their occupation number  $n_i = 1$  for N orbitals and  $n_i = 0$  for the rest.

To define effective potential  $V_{eff}$ , we assume the ground states solved from the non-interacting frame and the exact Hamiltonian are the same and compare the chemical potentials. The energy of non-interacting frame is

$$E_s[\rho] = T_s[\rho] + \int \rho(\mathbf{r}) V_{eff}(\mathbf{r}) d\mathbf{r}$$
(2.3.6)

and the universal term  $F[\rho]$  in (2.1.10) can be expressed conveniently to

$$F[\rho] = T_s[\rho] + E_H[\rho] + E_{XC}[\rho]$$
(2.3.7)

where the second term is Hartree functional which is electron-electron repulsion energy have the form

$$E_{H}[\rho] = \frac{1}{2} \iint \frac{\rho(r)\rho(r)}{|r-r'|} dr dr'$$
(2.3.8)

and the third term is called exchange-correlation energy; it contains the difference between T and  $T_s$ , but the exact form is unknown.

$$E_{xc}[\rho] = T[\rho] + V_{ee}[\rho] - T_s[\rho] - E_H[\rho]$$
(2.3.9)

The Euler equation for non-interaction frame becomes

$$\mu_s = V_{eff}(\mathbf{r}) + \frac{\delta T_s[\rho]}{\delta \rho(\mathbf{r})}$$
(2.3.10) and suppose  $\rho_s(\mathbf{r}) = \rho(\mathbf{r})$ , we have

$$\mu_s - \mu = V_{eff}(\mathbf{r}) - \left[ V_{ext}(\mathbf{r}) + \frac{\delta E_H[\rho]}{\delta \rho(\mathbf{r})} + \frac{\delta E_{XC}[\rho]}{\delta \rho(\mathbf{r})} \right] = \text{const.}$$
(2.3.11)

and we can define the KS effective potential as

$$V_{eff}(\mathbf{r}) = V_{ext}(\mathbf{r}) + \int \frac{\rho(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} d\mathbf{r}' + V_{xc}(\mathbf{r}) + const.$$
(2.3.12)

The Kohn-Sham method is an iteration process as follows. For a given effective potential  $V_{eff}$ , we can obtain  $\rho_s(\mathbf{r}) = \rho(\mathbf{r})$  without solving (2.3.10). Instead, we solve the simplified non-interacting Schrödinger equations which are the N one-electron equations

$$\hat{\mathbf{h}}(\boldsymbol{r})\phi_{i}(\boldsymbol{r}) = \left[-\frac{1}{2}\nabla^{2} + V_{eff}(\boldsymbol{r})\right]\phi_{i}(\boldsymbol{r}) = \varepsilon_{i}\phi_{i}(\boldsymbol{r}) \qquad (2.3.13)$$

which is called Kohn-Sham equation.

For non-interacting fermion systems, the wave function is antisymmetric. We can assume a simple form of single Slater determinant compose by the orbitals solved from (2.3.13) which is antisymmetric and satisfies (2.1.7) and (2.3.5)

$$\Psi = \frac{1}{\sqrt{N!}} \begin{vmatrix} \phi_1(r_1) & \phi_1(r_2) & \dots & \phi_1(r_N) \\ \phi_2(r_1) & \phi_2(r_2) & \dots & \phi_2(r_N) \\ \vdots & \vdots & \ddots & \vdots \\ \phi_N(r_1) & \phi_N(r_2) & \dots & \phi_N(r_N) \end{vmatrix}$$
(2.3.14)

To get  $\rho_s(\mathbf{r}) = \rho(\mathbf{r})$ , the iteration starts from guessing a trial density  $\rho_s(\mathbf{r})$  constructing the effective potential (2.3.12), and then solve the Kohn-Sham equation

(2.3.13) to get new orbitals set  $\{\phi_i(\mathbf{r})\}\$  and the associated  $\rho(\mathbf{r})\$  through (2.3.5). If the trial density and the new density are the same, this density and orbitals set is then the self-consistent solution. If they do not match, back to the start of iteration to construct a new effective potential and do the process again until it is close enough to true ground state density. Once we have the result, we can obtain the total energy from summing the energy in (2.3.13) and substitute into (2.1.10) together with (2.3.7).

$$E[\rho] = \int \rho(\mathbf{r}) V_{ext}(\mathbf{r}) d\mathbf{r} + T_s[\rho] + E_H[\rho] + E_{xc}[\rho]$$
$$= \sum_i^N \varepsilon_i - \frac{1}{2} \int \frac{\rho(\mathbf{r})\rho(\mathbf{r}')}{|\mathbf{r} - \mathbf{r}'|} d\mathbf{r} d\mathbf{r}' + E_{xc}[\rho] - \int V_{xc}(\mathbf{r})\rho(\mathbf{r}) d\mathbf{r} \qquad (2.3.15)$$

In general, the total energy is not the sum of the orbital energies.

Kohn-Sham DFT has an additional degree of freedom for electron-spin since the effective potential  $V_{eff}(\mathbf{r})$  is only spatial without information of spin. For each eigenvalue  $\varepsilon_i$ , there are two independent solutions sharing the same spatial part. The solutions are doubly degenerate and can be written as

$$\phi_i(\mathbf{r}, s) = \phi_{i\alpha}(\mathbf{r})\alpha(s) + \phi_{i\beta}(\mathbf{r})\beta(s)$$
(2.3.16)

so the wave functions satisfy density in (2.3.5). In spin-polarized case, the starting of the original iteration becomes guessing both spin-up and spin-down trial density.

Kohn-Sham method successfully makes DFT practically calculable. It approximates the N-electron system in non-interacting frame and simplifies the Hamiltonian to N one-electron effective Hamiltonians with single Slater determinant solution. The unknown is reduced from  $F[\rho]$  to  $E_{xc}[\rho]$ . The most important improvement is that KS method provides an easy iteration process to get the ground state quantities and thus KS-DFT has been widely developed and applied in few decades. However, due to the lack of accurate XC functional to describe the nonlocality of XC holes, KS-DFT has some qualitative failures [7][35-37].

#### 2.4 Thermally-Assisted-Occupation density functional theory

For the real N-electron system, the real ground state electron density can be represented for an interacting global external potential in terms of the natural orbitals  $\{\chi_i(\mathbf{r})\}\$  and natural orbital occupation numbers  $\{n_i\}$ ,

$$\rho_{FCI}(\mathbf{r}) = \sum_{i=1}^{\infty} n_i |\chi_i(\mathbf{r})|^2$$
(2.4.1)

where  $\{n_i\}$  follows conditions,

$$\sum_{i=1}^{\infty} n_i = N, \ 0 \le n_i \le 1$$
(2.4.2)

Comparing to the real density, the density in KS-DFT only has its orbitals fully occupied or unoccupied. Although we can obtain nature orbitals occupation numbers by the full configuration interaction (FCI) method, the computational cost is exponentially growing and thus unrealistic.

In 2012, Chai proposed a new method to correct errors in KS-DFT named thermalassisted-occupation density functional theory (TAO-DFT) [8]. TAO-DFT assumed a non-interacting thermal ensemble external potential representable electron density at a fictitious temperature  $\theta \equiv k_B T_{el}$  (where  $k_B$  is the Boltzmann constant,  $T_{el}$  is the temperature measured in absolute temperature). The density is set to be composed by infinite orbital sets with fractional occupation numbers to approach the real density which can correspondingly expressed as

$$\rho(\mathbf{r}) = \sum_{i=1}^{\infty} f_i |\psi_i(\mathbf{r})|^2$$
(2.4.3)

where  $f_i$  is Fermi-Dirac distribution

$$f_i = \{1 + exp[(\epsilon_i - \mu)/\theta]\}^{-1}$$



which follows the conditions

$$\sum_{i=1}^{\infty} f_i = N, \ 0 \le f_i \le 1$$
(2.4.5)

where  $\mu$  is the chemical potential chosen to conserve the number of electrons N.

From section 2.3, the universal functional can be expressed as (2.3.7). Since TAO-DFT has an additional degree of freedom  $\theta$ , we have to make  $F[\rho]$  a  $\theta$  related functional, start from (2.3.7),

$$F[\rho] = T_{s}[\rho] + E_{H}[\rho] + E_{xc}[\rho]$$

$$= A_{s}^{\theta}[\rho] + E_{H}[\rho] + (T[\rho] + V_{ee}[\rho] - A_{s}^{\theta}[\rho] - E_{H}[\rho])$$

$$= A_{s}^{\theta}[\rho] + E_{H}[\rho] + (T[\rho] + V_{ee}[\rho] - T_{s}[\rho] - E_{H}[\rho]) + (T_{s}[\rho] - A_{s}^{\theta}[\rho])$$

$$= A_{s}^{\theta}[\rho] + E_{H}[\rho] + E_{xc}[\rho] + E_{\theta}[\rho]$$
(2.4.6)

where  $A_s^{\theta}[\rho]$  is the non-interacting kinetic free energy at temperature  $\theta$ , and

$$E_{\theta}[\rho] \equiv T_{s}[\rho] - A_{s}^{\theta}[\rho] = A_{s}^{\theta=0}[\rho] - A_{s}^{\theta}[\rho]$$
(2.4.7)

This new universal functional will reduce to the universal functional (2.3.7) in KS-DFT at  $\theta = 0$  because the orbitals under fermi energy are fully occupied according to Fermi-Dirac distribution. Minimizing  $E[\rho]$  with respect to  $\rho(\mathbf{r})$  yields the Euler equation

$$\frac{\delta E[\rho]}{\delta \rho(r)} = \mu = \frac{\delta A_s^{\theta}[\rho]}{\delta \rho(r)} + v_{ext}(r) + \int \frac{\rho(r')}{|r-r'|} dr' + \frac{\delta E_{XC}[\rho]}{\delta \rho(r)} + \frac{\delta E_{\theta}[\rho]}{\delta \rho(r)}$$
(2.4.8)

where  $\mu$  is the chemical potential. Based on Mermin's theorems, a non-interacting system at temperature  $\theta$  will have minimum grand-canonical potential  $\Omega_s^{\theta}$  which be written as

$$\Omega_s^{\theta}[\rho_s] = A_s^{\theta}[\rho_s] + \int \rho_s(\mathbf{r})[V_s(\mathbf{r}) - \mu_s] d\mathbf{r}$$
(2.4.9)

where  $\mu_s$  is the chemical potential of the reference system. Minimizing  $\Omega_s^{\theta}$  yields the Euler equation

$$\mu_s = \frac{\delta A_s^{\theta}[\rho]}{\delta \rho(r)} + V_s(r) \tag{2.4.10}$$

Same as (2.3.11), if the both the fictitious density and the real density have the same  $\rho_s(\mathbf{r}) = \rho(\mathbf{r})$ , we can choose  $V_s(\mathbf{r})$  as

$$V_{s}(\mathbf{r}) = V_{ext}(\mathbf{r}) + \int \frac{\rho(\mathbf{r})}{|\mathbf{r}-\mathbf{r}'|} d\mathbf{r}' + \frac{\delta E_{XC}[\rho]}{\delta\rho(\mathbf{r})} + \frac{\delta E_{\theta}[\rho]}{\delta\rho(\mathbf{r})}$$
(2.4.11)

This new potential can replace the effective potential  $V_{eff}(\mathbf{r})$  in (2.3.13). To obtain a ground-state density using TAO-DFT, the iterating process is similar to one of KS-DFT. (i) choose a trial  $\rho_0(\mathbf{r})$  in (2.4.3) and construct  $V_s(\mathbf{r})$  using (2.4.11); (ii) solve Schrödinger equation

$$\left\{-\frac{1}{2}\nabla^2 + V_s(\boldsymbol{r})\right\}\psi_i(\boldsymbol{r}) = \epsilon_i\psi_i(\boldsymbol{r})$$
(2.4.12)

to get orbital energy  $\{\epsilon_i\}$  and non-interacting electron orbital set  $\{\psi_i(r)\}$ ; (iii) use  $\{\epsilon_i\}$  combining with the Fermi-Dirac distribution (2.4.4) and total number (2.4.5)

$$\sum_{i=1}^{\infty} \{1 + \exp[(\epsilon_i - \mu)/\theta]\}^{-1} = N$$
(2.4.13)

to find the chemical potential  $\mu$ ; (iv) determine  $\{f_i\}$  in (2.4.4) and new electron density

in (2.4.3). Keep iterating until this procedure reaches the convergence, and the exact non-interacting kinetic free energy  $A_s^{\theta}[\rho]$  can be expressed in terms of  $\{f_i, \psi_i(r)\}$ 

$$A_{s}^{\theta}[\{f_{i},\psi_{i}\}] = T_{s}^{\theta}[\{f_{i},\psi_{i}\}] - \frac{\theta}{k_{B}}S_{s}^{\theta}[\{f_{i}\}]$$
(2.4.14)

where  $T_s^{\theta}[\{f_i, \psi_i\}]$  is the sum of the kinetic energy

$$T_{s}^{\theta}[\{f_{i},\psi_{i}\}] = -\frac{1}{2}\sum_{i=1}^{\infty}f_{i}\int\psi_{i}^{*}(\boldsymbol{r})\nabla^{2}\psi_{i}(\boldsymbol{r})d\boldsymbol{r}$$
$$=\sum_{i=1}^{\infty}f_{i}\epsilon_{i}-\int\rho(\boldsymbol{r})V_{s}(\boldsymbol{r})d\boldsymbol{r} \qquad (2.4.15)$$

and the entropy functional reads

$$S_{s}^{\theta}[\{f_{i}\}] = -k_{B} \sum_{i=1}^{\infty} [f_{i} ln(f_{i}) + (1 - f_{i}) ln(1 - f_{i})]$$
(2.4.16)

When the fictitious temperature  $\theta$  is zero, TAO-DFT reduces to KS-DFT. The term  $\frac{\theta}{k_B}S_s^{\theta}[\{f_i\}]$  do not include information of wave function and is thus believed to describe the nonlocal static correlation where the original KS-DFT is unable to describe properly. Without this term, the degeneracy makes KS-DFT difficult to reach the global minimum dealing with the multi-reference systems. Due to the capability of including static correlation and reasonable efficiency, TAO-DFT is a promising tool to deal with large multi-reference system which high-level ab initio methods are stopped by the exponential computational cost.

#### 2.5 Computational Details

All the calculations are operated under quantum chemistry software Q-chem 4.3 [27][28]. From the length 3 to 8, the results are calculated by spin-restricted and spin-

unrestricted B3LYP with the basis set 6-31G\*. The singlet-triplet energy gap (ST gap) is defined as

$$E_{ST} = E_T - E_S$$

(2.21)

To compare to the reference, we obtained the energy difference between unrestricted triplet (UT) state, restricted triplet (RT) state, unrestricted singlet (US) state and restricted singlet (RS) state. The original ST gap becomes

$$E_{RT-RS} = E_{RT} - E_{RS}$$

$$E_{RT-US} = E_{RT} - E_{US}$$

$$E_{UT-RS} = E_{UT} - E_{RS}$$

$$E_{UT-U} = E_{UT} - E_{US}$$
(2.22)

The results of KS-DFT usually truncate to local minimum, we have to use different initial geometry of go through process with different conditions. The geometries of molecules are built in IQmol 2.13, optimized using universal force field, symmetrized in C2v point group. Each molecule we have only one geometry, but the processes are designed in at least 25 kinds of combination of different conditions. In Qchem, there are several kinds of initial guesses of self-consistent field such as reading from previous calculation, mixing 30% of HOMO and LUMO, core Hamiltonian, generalized Wolfsberg-Helmholtz, basis set projection; also, different SCF algorithms.

For the length 3 to 20, the calculations are based on TAO-LDA and TAO-B3LYP. The fictitious temperature  $\theta$  for TAO-LDA is set to be 7 mHartrees suggested by the founder where the orbital occupation perform similarly as the natural orbitals [8]. And so is the reason choosing  $\theta$  set to be 17.4 mHartrees [26]. The basis set of two methods is 6-31G\* and the spin is unrestricted.

For the longer length, the fictitious temperature  $\theta$  remains 7 mHartrees. The length calculated by the basis set 6-31G\* is up to 45 limited by the algorism due to the excessive virtual orbital, but can be up to 75 if the basis set is 6-31G. In convenient, basing on previous experience of TAO calculations, one geometry and one optimizing iteration process could be enough to obtain global minimum.

### **Chapter 3**

### Results



The details of the computational results are given in Table 3.1. Figure 3.1 shows the ST gaps of fused acene-azulenes as a function of their length, calculated using both spin-unrestricted and spin-restricted B3LYP as well as the result obtained from spinunrestricted TAO-B3LYP with its theta 17.4 mhartree. The unrestricted singlet and unrestricted triplet (UT-US) gaps reduce to almost zero rapidly due to the strong correlated effect. The difference between UT-US gaps and restricted triplet (RT)-UT gaps, namely RT-UT gaps basically remain the same as the length increase. However, the difference between UT-RS gaps oscillate unexpectedly due to unphysical symmetry-breaking effects. The reference [12] of triplet ground state from the previous study must be related to the UT-RS gaps without the non-monotonic decreasing part. By contrast, the ST gaps calculated using TAO-B3LYP decrease monotonically with increasing of the length.

Table 3.1: The unrestricted singlet (US), unrestricted triplet (UT), restricted singlet (RS) and restricted triplet (RT) state energy of fused-azulene-acene calculated by B3LYP/6-31G\* are given in Hartrees. The four kind of singlet-triplet energy gaps are in kcal/mol.

|   | US       | ΙT       | DC       | рт       |       |        | ST gaps |       |          |
|---|----------|----------|----------|----------|-------|--------|---------|-------|----------|
|   | 05       | UI       | KS       | KI       | UT-US | UT-RS  | RT-US   | RT-RS | Ref [12] |
| 3 | -539.45  | -539.43  | -539.45  | -539.43  | 12.46 | 12.46  | 14.83   | 14.83 | 12.45    |
| 4 | -693.08  | -693.08  | -693.08  | -693.08  | 0.08  | -2.85  | 2.85    | -0.08 | -2.77    |
| 5 | -846.72  | -846.72  | -846.71  | -846.72  | -0.02 | -8.65  | 3.01    | -5.61 | -8.53    |
| 6 | -1000.36 | -1000.36 | -1000.34 | -1000.36 | -0.08 | -10.55 | 3.14    | -7.34 | -10.61   |
| 7 | -1154.00 | -1154.00 | -1153.98 | -1153.99 | -0.10 | -10.86 | 3.23    | -7.54 |          |
| 8 | -1307.63 | -1307.63 | -1307.62 | -1307.63 | -0.10 | -10.53 | 3.30    | -7.14 |          |



Figure 3.1: Four kinds of singlet-triplet energy gaps of fused-azulene-acene, calculated by B3LYP and TAO-B3LYP ( $\theta = 17.4 \text{ mHartree}$ )/6-31G\* and reference data [12].

Figure 3.2 shows the ST gaps of n-acenes (GNR[1,n]) and fused azulene-acenes calculated using TAO-LDA and TAO-B3LYP in comparison. The exact values of each line are given in Table 3.2, Table 3.3, Table 3.4 and Table 3.5 respectively. In short length, the boundary defect greatly affects the original acenes, reducing the ST gaps. Though all of the results perform monotonically decreasing, TAO-B3LYP calculations seem to converge faster than the results of TAO-LDA. As the length increase, the ST gaps of fused azulene-acenes and acenes should be less different since the effect of the boundary defect becoming less relevant.



Figure 3.2: Singlet-triplet energy gap of acenes and fused azulene-acenes calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G\* and TAO-B3LYP ( $\theta = 17.4$  mHartree)/6-31G\*. Table 3.2: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fused-azulene-acene calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G\* are given in Hartrees. The ST gaps are given in kcal/mol.

|    | US       | UT       | ST gap |
|----|----------|----------|--------|
| 3  | -534.49  | -534.46  | 19.28  |
| 4  | -686.73  | -686.72  | 9.78   |
| 5  | -838.97  | -838.96  | 7.49   |
| 6  | -991.22  | -991.21  | 7.23   |
| 7  | -1143.46 | -1143.45 | 7.11   |
| 8  | -1295.70 | -1295.69 | 6.63   |
| 9  | -1447.94 | -1447.94 | 5.89   |
| 10 | -1600.19 | -1600.18 | 5.11   |
| 11 | -1752.43 | -1752.42 | 4.46   |
| 12 | -1904.67 | -1904.66 | 3.96   |
| 13 | -2056.91 | -2056.90 | 3.61   |
| 14 | -2209.15 | -2209.15 | 3.34   |
| 15 | -2361.39 | -2361.39 | 3.13   |
| 16 | -2513.63 | -2513.63 | 2.94   |
| 17 | -2665.88 | -2665.87 | 2.78   |
| 18 | -2818.12 | -2818.11 | 2.62   |
| 19 | -2970.36 | -2970.36 | 2.49 |
|----|----------|----------|------|
| 20 | -3122.60 | -3122.60 | 2.37 |



Table 3.3: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fusedazulene-acene calculated by TAO-B3LYP ( $\theta = 17.4 \text{ mHartree}$ )/6-31G\* are given in Hartrees. The ST gaps are given in kcal/mol. The restricted singlet (RS) state energy and the energy difference between RS and US (RS-US) are also listed in Hartrees in comparison.

|    | US       | UT       | ST gap | RS       | RS-US     |
|----|----------|----------|--------|----------|-----------|
| 3  | -539.40  | -539.37  | 16.23  | -539.40  | -6.62E-05 |
| 4  | -693.02  | -693.01  | 8.26   | -693.02  | -9.29E-04 |
| 5  | -846.64  | -846.63  | 6.10   | -846.64  | -8.08E-04 |
| 6  | -1000.27 | -1000.26 | 5.40   | -1000.27 | -1.53E-03 |
| 7  | -1153.89 | -1153.88 | 4.90   | -1153.89 | -1.41E-03 |
| 8  | -1307.52 | -1307.51 | 4.35   | -1307.52 | -1.79E-03 |
| 9  | -1461.14 | -1461.13 | 3.78   | -1461.14 | -1.80E-03 |
| 10 | -1614.76 | -1614.76 | 3.26   | -1614.76 | -2.00E-03 |
| 11 | -1768.38 | -1768.38 | 2.84   | -1768.38 | -2.55E-03 |
| 12 | -1922.01 | -1922.00 | 2.51   | -1922.01 | -1.50E-03 |
| 13 | -2075.63 | -2075.63 | 2.26   | -2075.63 | -2.81E-03 |
| 14 | -2229.25 | -2229.25 | 2.07   | -2229.25 | -6.50E-03 |
| 15 | -2382.88 | -2382.87 | 1.92   | -2382.88 | -1.17E-03 |
| 16 | -2536.50 | -2536.50 | 1.79   | -2536.50 | -1.14E-03 |
| 17 | -2690.12 | -2690.12 | 1.67   | -2690.12 | -1.12E-02 |
| 18 | -2843.75 | -2843.74 | 1.57   | -2843.75 | -1.03E-02 |
| 19 | -2997.37 | -2997.37 | 1.49   | -2997.37 | -1.31E-02 |
| 20 | -3150.99 | -3150.99 | 1.41   | -3150.99 | -1.51E-02 |

Table 3.4: The unrestricted singlet (US) and unrestricted triplet (UT) energy of linear acenes calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G\* are given in Hartrees. The ST gaps are given in kcal/mol.

|   | US      | UT      | ST gap |
|---|---------|---------|--------|
| 3 | -534.56 | -534.49 | 43.22  |
| 4 | -686.80 | -686.76 | 29.01  |

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| 5  | -839.04  | -839.01  | 19.60 |
|----|----------|----------|-------|
| 6  | -991.28  | -991.26  | 13.55 |
| 7  | -1143.52 | -1143.51 | 9.91  |
| 8  | -1295.76 | -1295.75 | 7.84  |
| 9  | -1448.01 | -1448.00 | 6.66  |
| 10 | -1600.25 | -1600.24 | 5.90  |
| 11 | -1752.49 | -1752.48 | 5.32  |
| 12 | -1904.73 | -1904.72 | 4.82  |
| 13 | -2056.97 | -2056.97 | 4.37  |
| 14 | -2209.21 | -2209.21 | 3.98  |
| 15 | -2361.46 | -2361.45 | 3.65  |
| 16 | -2513.70 | -2513.69 | 3.37  |
| 17 | -2665.94 | -2665.93 | 3.14  |
| 18 | -2818.18 | -2818.18 | 2.94  |
| 19 | -2970.42 | -2970.42 | 2.77  |
| 20 | -3122.66 | -3122.66 | 2.62  |

Table 3.5: The unrestricted singlet (US) and unrestricted triplet (UT) energy of linear acenes calculated by TAO-B3LYP ( $\theta = 17.4$  mHartree)/6-31G\* are given in Hartrees. The ST gaps are given in kcal/mol.

|    | US       | UT       | ST gap |
|----|----------|----------|--------|
| 3  | -539.47  | -539.41  | 40.44  |
| 4  | -693.09  | -693.05  | 27.27  |
| 5  | -846.71  | -846.68  | 18.74  |
| 6  | -1000.34 | -1000.31 | 13.31  |
| 7  | -1153.96 | -1153.94 | 9.89   |
| 8  | -1307.58 | -1307.57 | 7.73   |
| 9  | -1461.20 | -1461.19 | 6.30   |
| 10 | -1614.83 | -1614.82 | 5.31   |
| 11 | -1768.45 | -1768.44 | 4.57   |
| 12 | -1922.07 | -1922.07 | 3.99   |
| 13 | -2075.70 | -2075.69 | 3.53   |
| 14 | -2229.32 | -2229.31 | 3.16   |
| 15 | -2382.94 | -2382.94 | 2.85   |
| 16 | -2536.57 | -2536.56 | 2.60   |
| 17 | -2690.19 | -2690.18 | 2.39   |

| 18 | -2843.81 | -2843.81 | 2.22 |
|----|----------|----------|------|
| 19 | -2997.43 | -2997.43 | 2.07 |
| 20 | -3151.06 | -3151.05 | 1.94 |



To compare the result to acenes, we expand the system to n being 46 (see Table 3.6) and 75 (see Table 3.7) calculated by TAO-LDA ( $\theta = 7$  mHartree) with the basis set 6-31G\* and 6-31G since the 6-31G\* calculation cannot truncate correctly. From Figure 3.3 we see that the results of this two basis have only little difference, thus we choose the 6-31G result comparing with acenes in Figure 3.4. The difference between fused azulene-acenes and acenes does decrease as the length increase.



Figure 3.3: Singlet-triplet energy gap of fused azulene-acenes for n from 3 to 46 calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G\* and for n from 3 to 75 calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G.



Figure 3.4: Singlet-triplet energy gap for the longer acenes [13] and fused azuleneacenes calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G.

Table 3.6: The unrestricted singlet (US) and unrestricted triplet (UT) energy of fusedazulene-acene and acenes calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G\* are given in Hartrees. The ST gaps of both fused-azulene-acene and acene are given in kcal/mol.

|    | acene    |          |        |        |
|----|----------|----------|--------|--------|
|    | US       | UT       | ST gap | ST gap |
| 3  | -534.49  | -534.46  | 19.28  | 43.22  |
| 4  | -686.73  | -686.72  | 9.78   | 29.01  |
| 5  | -838.97  | -838.96  | 7.49   | 19.60  |
| 6  | -991.22  | -991.21  | 7.23   | 13.55  |
| 7  | -1143.46 | -1143.45 | 7.11   | 9.91   |
| 8  | -1295.70 | -1295.69 | 6.63   | 7.85   |
| 9  | -1447.94 | -1447.94 | 5.89   | 6.66   |
| 10 | -1600.19 | -1600.18 | 5.11   | 5.91   |
| 11 | -1752.43 | -1752.42 | 4.46   | 5.32   |
| 12 | -1904.67 | -1904.66 | 3.96   | 4.82   |
| 13 | -2056.91 | -2056.90 | 3.61   | 4.38   |
| 14 | -2209.15 | -2209.15 | 3.34   | 3.98   |
| 15 | -2361.39 | -2361.39 | 3.13   | 3.65   |
| 16 | -2513.63 | -2513.63 | 2.94   | 3.37   |
| 17 | -2665.88 | -2665.87 | 2.78   | 3.14   |
| 18 | -2818.12 | -2818.11 | 2.62   | 2.94   |
| 19 | -2970.36 | -2970.36 | 2.49   | 2.77   |



| 20 | -3122.60 | -3122.60 | 2.36 | 2.62 |
|----|----------|----------|------|------|
| 21 | -3274.84 | -3274.84 | 2.25 | 2.49 |
| 22 | -3427.08 | -3427.08 | 2.15 | 2.37 |
| 23 | -3579.33 | -3579.32 | 2.06 | 2.25 |
| 24 | -3731.57 | -3731.56 | 1.97 | 2.15 |
| 25 | -3883.81 | -3883.81 | 1.89 | 2.06 |
| 26 | -4036.05 | -4036.05 | 1.82 | 1.98 |
| 27 | -4188.29 | -4188.29 | 1.76 | 1.90 |
| 28 | -4340.53 | -4340.53 | 1.69 | 1.83 |
| 29 | -4492.77 | -4492.77 | 1.64 | 1.76 |
| 30 | -4645.02 | -4645.01 | 1.58 | 1.70 |
| 31 | -4797.26 | -4797.25 | 1.53 | 1.64 |
| 32 | -4949.50 | -4949.50 | 1.49 | 1.59 |
| 33 | -5101.74 | -5101.74 | 1.44 | 1.54 |
| 34 | -5253.98 | -5253.98 | 1.40 | 1.49 |
| 35 | -5406.22 | -5406.22 | 1.36 | 1.45 |
| 36 | -5558.46 | -5558.46 | 1.32 | 1.40 |
| 37 | -5710.71 | -5710.70 | 1.29 | 1.36 |
| 38 | -5862.95 | -5862.95 | 1.26 | 1.33 |
| 39 | -6015.19 | -6015.19 | 1.22 | 1.29 |
| 40 | -6167.43 | -6167.43 | 1.19 | 1.26 |
| 41 | -6319.67 | -6319.67 | 1.17 | 1.23 |
| 42 | -6471.91 | -6471.91 | 1.14 | 1.20 |
| 43 | -6624.16 | -6624.15 | 1.11 | 1.17 |
| 44 | -6776.40 | -6776.40 | 1.09 | 1.14 |
| 45 | -6928.64 | -6928.64 | 1.06 | 1.11 |
| 46 | -7080.88 | -7080.88 | 1.04 | 1.09 |
|    |          |          |      |      |

Biradical character or even polyradical character of molecules can be judged quantitively by natural orbital occupation numbers (NOONs) [23]. The NOONs can offer the evidence of polyradical character of molecules, since the NOONs are either 0 (fully unoccupied) or 2 (fully occupied) in the single-reference system. NOONs between 2 and 0 may be interpreted as fractionally occupied electrons. In Figure 3.6, we plot the active orbital occupation numbers for the lowest singlet state of fused azuleneacene as a function of the ribbon length, calculated using spin-restricted TAO-LDA( $\theta$  = 7 mHartree)/6-31G. Here, the highest occupied molecular orbital (HOMO) is the (N/2)th orbital, and the lowest unoccupied molecular orbital (LUMO) is the (N/2 + 1)th orbital, with the N being the number of the electrons in fused azulene-acene. As shown, the number of fractionally occupied orbitals increasing with the increase of ribbon length, supporting the fused azulene-acenes have polyradical character similar to acenes.



Figure 3.5: Active orbital occupation numbers (HOMO-13, ..., HOMO-1, HOMO, LUMO, LUMO-1, ..., and LUMO-13) as a function of the fused azulene-acene length calculated using spin-restricted TAO-LDA ( $\theta = 7$  mHartree)/6-31G.

A quantitative criterion to measure the static correlation is the symmetrized von Neumann entropy [17][24].

$$S = -\frac{1}{2}\sum_{i}[f_{i}ln(f_{i}) + (1 - f_{i})ln(1 - f_{i})]$$
(3.1)

which is the symmetrized form of the von Neumann entropy,  $S = -\sum_i f_i ln(f_i)$  [25]. The von Neumann entropy, a scalar extracted from the occupation number array, is a wave function based criterion to measure the static correlation error. Because the symmetrized von Neumann entropy are zero for single-reference system, the magnitude can be referred to as an index to judge the static correlation in the systems. Although symmetrized von Neumann entropy lost some detailed information in the process of extraction, the one-dimensional number character also provide a simple way to measure the degree of polyradical or severeness of static correlation. As Figure 3.6 shown, the slope of the symmetrized von Neumann entropy of fused azulene-acenes and acenes are the same, but the difference between two line is a constant for the long ribbon length. According to active orbital occupation numbers of the lowest singlet state of the spin-restricted fused azulene-acene (Figure 3.6), the patterns of the fractional occupation of the two are similar, though the occupation numbers of fused azulene-acene turns to fractional earlier than that of acenes [13]. This may support the translation of the symmetrized von Neumann entropy.



Figure 3.6: Symmetrized von Neumann entropy for the lowest singlet state of fused azulene-acenes and acenes calculated using spin-restricted TAO-LDA ( $\theta = 7$  mHartree)/6-31G.

Table 3.7: The unrestricted singlet (US) and the unrestricted triplet (UT) energy of fused azulene-acenes calculated by TAO-LDA ( $\theta = 7$  mHartree)/6-31G are given in Hartrees. The ST gaps of fused azulene-acene, acenes [13] and  $\Delta$  are given in kcal/mol where  $\Delta$  is the difference between ST gaps of fused azulene-acene and acenes. The dipole moment of US and UT and the singlet-triplet dipole moment gap are given in debye. The symmetrized von Neumann entropy of both fused azulene-acene and acenes [13] are given.

|    | fused-a  | azulene-acer | ne     | acene  |       | fuse  | d-azule | ne-acene |      | acene |
|----|----------|--------------|--------|--------|-------|-------|---------|----------|------|-------|
| _  | US       | UT           | ST gap | ST gap | Δ     | μ(US) | μ(UT)   | μ(UT-US) | svNe | svNe  |
| 3  | -534.36  | -534.33      | 19.43  | 43.22  | 23.79 | 2.63  | -0.04   | -2.66    | 0.62 | 0.03  |
| 4  | -686.56  | -686.55      | 9.80   | 29.01  | 19.21 | 2.98  | 0.80    | -2.17    | 1.24 | 0.15  |
| 5  | -838.77  | -838.75      | 7.48   | 19.60  | 12.12 | 2.80  | 1.89    | -0.90    | 1.39 | 0.40  |
| 6  | -990.97  | -990.96      | 7.19   | 13.55  | 6.36  | 2.65  | 2.89    | 0.24     | 1.42 | 0.75  |
| 7  | -1143.18 | -1143.17     | 7.05   | 9.91   | 2.86  | 2.62  | 3.56    | 0.94     | 1.46 | 1.08  |
| 8  | -1295.38 | -1295.37     | 6.57   | 7.85   | 1.28  | 2.70  | 3.89    | 1.19     | 1.55 | 1.34  |
| 9  | -1447.59 | -1447.58     | 5.84   | 6.66   | 0.82  | 2.85  | 4.02    | 1.16     | 1.71 | 1.52  |
| 10 | -1599.79 | -1599.78     | 5.08   | 5.91   | 0.83  | 3.06  | 4.08    | 1.02     | 1.92 | 1.67  |
| 11 | -1751.99 | -1751.99     | 4.42   | 5.32   | 0.90  | 3.27  | 4.13    | 0.85     | 2.15 | 1.98  |
| 12 | -1904.20 | -1904.19     | 3.93   | 4.82   | 0.89  | 3.48  | 4.20    | 0.72     | 2.36 | 2.16  |
| 13 | -2056.40 | -2056.39     | 3.57   | 4.38   | 0.81  | 3.67  | 4.30    | 0.63     | 2.56 | 2.36  |
| 14 | -2208.60 | -2208.60     | 3.30   | 3.98   | 0.68  | 3.85  | 4.42    | 0.57     | 2.74 | 2.55  |
| 15 | -2360.81 | -2360.80     | 3.08   | 3.65   | 0.57  | 4.01  | 4.55    | 0.54     | 2.93 | 2.75  |
| 16 | -2513.01 | -2513.01     | 2.90   | 3.37   | 0.47  | 4.17  | 4.69    | 0.51     | 3.11 | 2.94  |
| 17 | -2665.21 | -2665.21     | 2.73   | 3.14   | 0.41  | 4.34  | 4.83    | 0.49     | 3.30 | 3.13  |
| 18 | -2817.42 | -2817.41     | 2.58   | 2.94   | 0.36  | 4.50  | 4.97    | 0.48     | 3.49 | 3.31  |
| 19 | -2969.62 | -2969.62     | 2.45   | 2.77   | 0.32  | 4.66  | 5.12    | 0.46     | 3.67 | 3.50  |
| 20 | -3121.83 | -3121.82     | 2.32   | 2.62   | 0.30  | 4.83  | 5.26    | 0.43     | 3.86 | 3.69  |
| 21 | -3274.03 | -3274.03     | 2.21   | 2.49   | 0.28  | 4.99  | 5.40    | 0.41     | 4.05 | 3.88  |
| 22 | -3426.23 | -3426.23     | 2.11   | 2.37   | 0.26  | 5.15  | 5.55    | 0.40     | 4.24 | 4.07  |
| 23 | -3578.44 | -3578.43     | 2.02   | 2.25   | 0.23  | 5.32  | 5.69    | 0.38     | 4.43 | 4.26  |
| 24 | -3730.64 | -3730.64     | 1.94   | 2.15   | 0.21  | 5.48  | 5.84    | 0.36     | 4.62 | 4.44  |
| 25 | -3882.84 | -3882.84     | 1.86   | 2.06   | 0.20  | 5.64  | 5.99    | 0.35     | 4.81 | 4.63  |
| 26 | -4035.05 | -4035.04     | 1.79   | 1.98   | 0.19  | 5.80  | 6.14    | 0.34     | 5.00 | 4.82  |
| 27 | -4187.25 | -4187.25     | 1.72   | 1.90   | 0.18  | 5.95  | 6.28    | 0.33     | 5.19 | 5.01  |
| 28 | -4339.46 | -4339.45     | 1.66   | 1.83   | 0.17  | 6.12  | 6.43    | 0.31     | 5.38 | 5.20  |
| 29 | -4491.66 | -4491.66     | 1.61   | 1.76   | 0.15  | 6.28  | 6.58    | 0.30     | 5.56 | 5.39  |
| 30 | -4643.86 | -4643.86     | 1.55   | 1.70   | 0.15  | 6.43  | 6.72    | 0.30     | 5.75 | 5.58  |
| 31 | -4796.07 | -4796.06     | 1.50   | 1.64   | 0.14  | 6.59  | 6.87    | 0.28     | 5.94 | 5.77  |

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|----|-----------|-----------|------|------|------|-------|-------|-------------|----------|
| 32 | -4948.27  | -4948.27  | 1.46 | 1.59 | 0.13 | 6.74  | 7.01  | 0.27 6.13   | 5.95     |
| 33 | -5100.47  | -5100.47  | 1.41 | 1.54 | 0.13 | 6.89  | 7.16  | 0.27 6.32   | 6.14     |
| 34 | -5252.68  | -5252.68  | 1.37 | 1.49 | 0.12 | 7.05  | 7.31  | 0.26 6.51   | 6.33     |
| 35 | -5404.88  | -5404.88  | 1.33 | 1.45 | 0.12 | 7.21  | 7.46  | 0.25 6.70   | 6.52     |
| 36 | -5557.08  | -5557.08  | 1.30 | 1.40 | 0.10 | 7.37  | 7.61  | 0.23 6.89   | 6.71     |
| 37 | -5709.29  | -5709.29  | 1.26 | 1.36 | 0.10 | 7.52  | 7.75  | 0.24 7.07   | 6.90     |
| 38 | -5861.49  | -5861.49  | 1.23 | 1.33 | 0.10 | 7.67  | 7.90  | 0.22 7.26   | 7.09     |
| 39 | -6013.70  | -6013.69  | 1.20 | 1.29 | 0.09 | 7.83  | 8.05  | 0.22 7.45   | 7.27     |
| 40 | -6165.90  | -6165.90  | 1.17 | 1.26 | 0.09 | 7.98  | 8.19  | 0.22 7.64   | 7.46     |
| 41 | -6318.10  | -6318.10  | 1.14 | 1.23 | 0.09 | 8.13  | 8.34  | 0.21 7.83   | 7.65     |
| 42 | -6470.31  | -6470.30  | 1.12 | 1.20 | 0.08 | 8.28  | 8.49  | 0.21 8.02   | 7.84     |
| 43 | -6622.51  | -6622.51  | 1.09 | 1.17 | 0.08 | 8.43  | 8.64  | 0.21 8.21   | 8.03     |
| 44 | -6774.71  | -6774.71  | 1.07 | 1.14 | 0.07 | 8.57  | 8.78  | 0.21 8.40   | 8.22     |
| 45 | -6926.92  | -6926.92  | 1.04 | 1.11 | 0.07 | 8.73  | 8.94  | 0.21 8.59   | 8.41     |
| 46 | -7079.12  | -7079.12  | 1.02 | 1.09 | 0.07 | 8.88  | 9.07  | 0.20 8.77   | 8.59     |
| 47 | -7231.33  | -7231.32  | 1.00 | 1.07 | 0.07 | 9.02  | 9.21  | 0.19 8.96   | 8.78     |
| 48 | -7383.53  | -7383.53  | 0.98 | 1.04 | 0.06 | 9.16  | 9.35  | 0.18 9.15   | 8.97     |
| 49 | -7535.73  | -7535.73  | 0.96 | 1.02 | 0.06 | 9.33  | 9.49  | 0.16 9.34   | 9.16     |
| 50 | -7687.94  | -7687.93  | 0.94 | 1.00 | 0.06 | 9.48  | 9.64  | 0.16 9.53   | 9.35     |
| 51 | -7840.14  | -7840.14  | 0.92 | 0.98 | 0.06 | 9.62  | 9.80  | 0.17 9.72   | 9.54     |
| 52 | -7992.34  | -7992.34  | 0.90 | 0.96 | 0.06 | 9.77  | 9.93  | 0.17 9.91   | 9.73     |
| 53 | -8144.55  | -8144.55  | 0.89 | 0.94 | 0.05 | 9.91  | 10.08 | 0.17 10.10  | 9.92     |
| 54 | -8296.75  | -8296.75  | 0.87 | 0.92 | 0.05 | 10.04 | 10.22 | 0.18 10.28  | 10.10    |
| 55 | -8448.95  | -8448.95  | 0.85 | 0.91 | 0.06 | 10.20 | 10.37 | 0.17 10.47  | 10.29    |
| 56 | -8601.16  | -8601.16  | 0.84 | 0.89 | 0.05 | 10.34 | 10.50 | 0.16 10.66  | 10.48    |
| 57 | -8753.36  | -8753.36  | 0.83 | 0.87 | 0.04 | 10.49 | 10.67 | 0.17 10.85  | 10.67    |
| 58 | -8905.57  | -8905.56  | 0.81 | 0.86 | 0.05 | 10.66 | 10.81 | 0.16 11.04  | 10.86    |
| 59 | -9057.77  | -9057.77  | 0.80 | 0.84 | 0.04 | 10.82 | 10.93 | 0.11 11.23  | 11.05    |
| 60 | -9209.97  | -9209.97  | 0.78 | 0.83 | 0.05 | 10.93 | 11.07 | 0.14 11.42  | 11.23    |
| 61 | -9362.18  | -9362.18  | 0.77 | 0.82 | 0.05 | 11.10 | 11.22 | 0.12 11.61  | 11.42    |
| 62 | -9514.38  | -9514.38  | 0.76 | 0.80 | 0.04 | 11.23 | 11.35 | 0.13 11.79  | 11.61    |
| 63 | -9666.58  | -9666.58  | 0.75 | 0.79 | 0.04 | 11.46 | 11.50 | 0.04 11.98  | 11.80    |
| 64 | -9818.79  | -9818.79  | 0.74 | 0.78 | 0.04 | 11.68 | 11.65 | -0.03 12.17 | 11.99    |
| 65 | -9970.99  | -9970.99  | 0.72 | 0.76 | 0.04 | 11.65 | 11.83 | 0.18 12.36  | 12.18    |
| 66 | -10123.20 | -10123.19 | 0.71 | 0.75 | 0.04 | 11.81 | 11.93 | 0.13 12.55  | 12.37    |
| 67 | -10275.40 | -10275.40 | 0.70 | 0.74 | 0.04 | 11.93 | 12.11 | 0.18 12.74  | 12.56    |
| 68 | -10427.60 | -10427.60 | 0.69 | 0.73 | 0.04 | 12.07 | 12.39 | 0.32 12.93  | 12.74    |
| 69 | -10579.81 | -10579.81 | 0.68 | 0.72 | 0.04 | 12.25 | 12.49 | 0.24 13.12  | 12.93    |

|    |           |           |      |      |            |       | 14 A             |
|----|-----------|-----------|------|------|------------|-------|------------------|
| 70 | -10732.01 | -10732.01 | 0.67 | 0.71 | 0.04 12.37 | 12.48 | 0.11 13.31 13.12 |
| 71 | -10884.21 | -10884.21 | 0.66 | 0.70 | 0.04 12.49 | 12.61 | 0.12 13.49 13.31 |
| 72 | -11036.42 | -11036.42 | 0.66 | 0.69 | 0.03 12.65 | 12.75 | 0.10 13.68 13.50 |
| 73 | -11188.62 | -11188.62 | 0.65 | 0.68 | 0.03 12.83 | 12.89 | 0.06 13.87 13.69 |
| 74 | -11340.82 | -11340.82 | 0.64 | 0.67 | 0.03 12.98 | 13.05 | 0.07 14.06 13.88 |
| 75 | -11493.03 | -11493.03 | 0.63 | 0.66 | 0.03 13.12 | 13.18 | 0.06 14.25 14.06 |

From Figure 3.7 to Figure 3.10, we show the real-space representation of shortest four lowest singlet states of fused azulene-acene obtained with spin-restricted TAO-LDA since we find a curve crossing behavior in the approach to single occupation with increasing length. The shape of orbitals of HOMO and LUMO exchange at the point where the curve cross. The curve crossing behavior may be an artifact showing the limitation of TAO-LDA (with a system-independent  $\theta$ ) [13]. In addition of mainly localized at the edge of acenes in previous studies [13][17], the orbital of long-chain fused azulene-acene shown in Appendix B have nodes, and the amount of nodes increases with the length periodically.



Figure 3.7: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=3) with their occupation number 1.8157 and 0.1841



Figure 3.8: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=4) with their occupation number 1.3877 and 0.6119



Figure 3.9: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=5) with their occupation number 1.1038 and 0.8961



Figure 3.10: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=6) with their occupation number 1.0707 and 0.9301

Polarity can affect ST gap on the aromatic compound [14]. To study the detail of how the ST gaps are tuned, in Figure 3.7, we show the differences between ST gap of acene and fused azulene-acene and the dipole moment singlet triplet gap. The dipole moment of both unrestricted singlet state and unrestricted triplet state increase monotonically in Table 3.7, though the polarity inverse when n less than 6. In the short length, the two quantities have negative correlation. As the length increase, polarity has less influence in tuning the ST gap, though there is zigzag on the line, which we do not know that it is error during converging or the character of this system. Since we only use one geometry and one iteration process, the failed results may be truncated to local minimum, though other properties perform well or be too small to be realized.



Figure 3.11: Differences between STgap of n-acenes [13] and fused azulene-acene and dipole moment difference between single and triplet state of fused azulene-acene calculating using spin-unrestricted TAO-LDA ( $\theta = 7$  mHartree)/6-31G.

## Chapter 4

### Conculsion



TAO-LDA is a more efficient method and also greatly corrects static correlation error in Kohn-Sham LDA. The expensive calculation cost makes TAO-LDA easily applied on larger molecules. In this study, it is used to explore electronic properties of linear isomers of polyacenes which have its two ends replaced by 7 and 5 carbon rings. We predict that the fused azulene-acene should be singlet ground state instead of triplet ground state, and also reproduce the KS calculations to show that the results varies under different conditions with different physical meaning. Fractional orbital occupation numbers and nonzero symmetrized von Neumann entropy can be the evidence of polyradical properties of this acene-like system. Fused azulene-acene do has similar orbital occupation structure to acene. Besides, the results calculated by TAO-LDA provides a way to tune the ST gap by adding dipole moment. However, the affect is limited for large molecules.

In future, this system can be expanded to 2D finite size of other combination of 5 and 7 rings, though it is hard to deal with lots of combinations on the edge. Also it could be hard to compare with its zigzag graphene nanoribbons isomers because the structure and polarity. Other way to create polarity flipping could be dosing different atoms in acene to tune ST gaps for wider applications.

## **Chapter 5**

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## Appendix A: Active orbital occupation numbers for the lowest singlet states of fused azulene-acene

Table A: Active orbital occupation numbers (HOMO-13, ..., HOMO-1, LUMO-1, ..., LUMO-13) for the lowest singlet states of fused azulene-acene, calculated by spin-restricted TAO-LDA ( $\theta = 7$  mHartree), using the 6-31G basis set.

|          | $f_{H-13}$ | $f_{H-12}$ | <i>f</i> <sub><i>H</i>-11</sub> | $f_{H-10}$ | $f_{H-9}$ | $f_{H-8}$ | $f_{H-7}$ | $f_{H-6}$ | $f_{H-5}$ | $f_{H-4}$ | $f_{H-3}$ | $f_{H-2}$ | $f_{H-1}$ |
|----------|------------|------------|---------------------------------|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| 3        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9999    | 1.8156    |
| 4        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9999    | 1.9998    | 1.3873    |
| 5        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9998    | 1.9991    | 1.1029    |
| 6        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9998    | 1.9949    | 1.0703    |
| 7        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9999    | 1.9998    | 1.9810    | 1.1877    |
| 8        | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9998    | 1.9995    | 1.9474    | 1.2739    |
| 10       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9998    | 1.9982    | 1.8848    | 1.3403    |
| 10       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.99999   | 1.9998    | 1.9952    | 1./914    | 1.3923    |
| 11       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 2.0000    | 1.9998    | 1.9996    | 1.988/    | 1.0/5/    | 1.4319    |
| 12       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 1.99999   | 1.9998    | 1.9990    | 1.9/00    | 1.5498    | 1.4020    |
| 13       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 2.0000    | 1.9990    | 1.9996    | 1.9977    | 1.9308    | 1.4002    | 1.4230    |
| 14       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 1 0000    | 1.9998    | 1.9990    | 1.9952    | 1.9274    | 1.5049    | 1.3101    |
| 16       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 1 9998    | 1 9998    | 1.9985    | 1 9844    | 1.8365    | 1.5200    | 1.2007    |
| 17       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 2.0000    | 1.9998    | 1.9997    | 1.9973    | 1.9745    | 1.7762    | 1.5435    | 1.0371    |
| 18       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 1.9999    | 1.9998    | 1.9994    | 1.9952    | 1.9605    | 1.7086    | 1.5528    | 1.0404    |
| 19       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 2.0000    | 1.9998    | 1.9998    | 1.9989    | 1.9922    | 1.9418    | 1.6362    | 1.5608    | 1.1017    |
| 20       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 1.9999    | 1.9998    | 1.9997    | 1.9981    | 1.9877    | 1.9179    | 1.5678    | 1.5615    | 1.1546    |
| 21       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 1.9999    | 1.9998    | 1.9995    | 1.9970    | 1.9815    | 1.8886    | 1.5740    | 1.4869    | 1.2005    |
| 22       | 2.0000     | 2.0000     | 2.0000                          | 2.0000     | 1.9998    | 1.9998    | 1.9991    | 1.9953    | 1.9732    | 1.8539    | 1.5794    | 1.4140    | 1.2403    |
| 23       | 2.0000     | 2.0000     | 2.0000                          | 1.9999     | 1.9998    | 1.9997    | 1.9986    | 1.9929    | 1.9624    | 1.8142    | 1.5841    | 1.3442    | 1.2751    |
| 24       | 2.0000     | 2.0000     | 2.0000                          | 1.9999     | 1.9998    | 1.9995    | 1.9978    | 1.9896    | 1.9489    | 1.7700    | 1.5884    | 1.3057    | 1.2782    |
| 25       | 2.0000     | 2.0000     | 2.0000                          | 1.9998     | 1.9998    | 1.9993    | 1.9968    | 1.9852    | 1.9322    | 1.7223    | 1.5922    | 1.3326    | 1.2164    |
| 26       | 2.0000     | 2.0000     | 1.9999                          | 1.9998     | 1.9997    | 1.9989    | 1.9953    | 1.9796    | 1.9124    | 1.6719    | 1.5956    | 1.3564    | 1.1592    |
| 27       | 2.0000     | 2.0000     | 1.9999                          | 1.9998     | 1.9996    | 1.9983    | 1.9933    | 1.9724    | 1.8893    | 1.6197    | 1.5987    | 1.3775    | 1.1063    |
| 28       | 2.0000     | 1.9999     | 1.9998                          | 1.9998     | 1.9994    | 1.9976    | 1.9907    | 1.9636    | 1.8629    | 1.6015    | 1.5665    | 1.3964    | 1.0577    |
| 29       | 2.0000     | 1.9999     | 1.9998                          | 1.9997/    | 1.9991    | 1.9966    | 1.9874    | 1.9530    | 1.8335    | 1.6041    | 1.5133    | 1.4133    | 1.0130    |
| 30       | 2.0000     | 1.9999     | 1.9998                          | 1.9996     | 1.9986    | 1.9953    | 1.9832    | 1.9403    | 1.8013    | 1.6064    | 1.4606    | 1.4285    | 1.0378    |
| 31       | 1.99999    | 1.9998     | 1.9998                          | 1.9994     | 1.9981    | 1.9936    | 1.9/81    | 1.9256    | 1.7007    | 1.6086    | 1.4423    | 1.4090    | 1.0//1    |
| 32<br>22 | 1.9999     | 1.9998     | 1.9997                          | 1.9992     | 1.99/4    | 1.9915    | 1.9/19    | 1.9088    | 1./29/    | 1.0105    | 1.454/    | 1.3390    | 1.1131    |
| 22<br>24 | 1.9999     | 1.9998     | 1.9990                          | 1.9989     | 1.9903    | 1.9000    | 1.9044    | 1.009/    | 1.0911    | 1.0124    | 1.4000    | 1.5108    | 1.1400    |
| 35       | 1.9998     | 1.9998     | 1 9993                          | 1 9979     | 1.9933    | 1.9830    | 1.9357    | 1.8085    | 1.6156    | 1.6105    | 1.4705    | 1.2040    | 1.1701    |
| 36       | 1 9998     | 1 9996     | 1 9990                          | 1 9972     | 1.9920    | 1.9770    | 1.9430    | 1.8200    | 1.6170    | 1.5693    | 1 4943    | 1.2200    | 1.2037    |
| 37       | 1.9998     | 1.9995     | 1.9987                          | 1.9964     | 1.9898    | 1.9714    | 1.9208    | 1.7930    | 1.6184    | 1.5279    | 1.5023    | 1.2524    | 1.1393    |
| 38       | 1.9997     | 1.9993     | 1.9983                          | 1.9953     | 1.9872    | 1.9650    | 1.9062    | 1.7644    | 1.6196    | 1.5096    | 1.4868    | 1.2738    | 1.1020    |
| 39       | 1.9997     | 1.9991     | 1.9977                          | 1.9940     | 1.9841    | 1.9576    | 1.8900    | 1.7344    | 1.6208    | 1.5163    | 1.4462    | 1.2936    | 1.0669    |
| 40       | 1.9995     | 1.9988     | 1.9971                          | 1.9924     | 1.9804    | 1.9492    | 1.8722    | 1.7031    | 1.6219    | 1.5226    | 1.4062    | 1.3119    | 1.0338    |
| 41       | 1.9994     | 1.9985     | 1.9963                          | 1.9906     | 1.9761    | 1.9396    | 1.8530    | 1.6710    | 1.6229    | 1.5283    | 1.3672    | 1.3287    | 1.0059    |
| 42       | 1.9992     | 1.9981     | 1.9953                          | 1.9884     | 1.9711    | 1.9290    | 1.8324    | 1.6381    | 1.6239    | 1.5337    | 1.3444    | 1.3293    | 1.0367    |
| 43       | 1.9990     | 1.9976     | 1.9941                          | 1.9858     | 1.9654    | 1.9172    | 1.8104    | 1.6248    | 1.6047    | 1.5387    | 1.3589    | 1.2925    | 1.0656    |
| 44       | 1.9987     | 1.9969     | 1.9928                          | 1.9828     | 1.9590    | 1.9043    | 1.7872    | 1.6256    | 1.5710    | 1.5434    | 1.3724    | 1.2571    | 1.0928    |
| 45       | 1.9984     | 1.9962     | 1.9912                          | 1.9793     | 1.9518    | 1.8902    | 1.7628    | 1.6264    | 1.5478    | 1.5372    | 1.3849    | 1.2229    | 1.1182    |
| 46       | 1.9979     | 1.9953     | 1.9893                          | 1.9753     | 1.9438    | 1.8750    | 1.7376    | 1.6271    | 1.5518    | 1.5036    | 1.3966    | 1.1901    | 1.1420    |
| 47       | 1.9974     | 1.9943     | 1.9871                          | 1.9708     | 1.9349    | 1.8586    | 1.7114    | 1.6278    | 1.5556    | 1.4702    | 1.4075    | 1.1644    | 1.1587    |
| 48       | 1.9968     | 1.9930     | 1.9846                          | 1.9658     | 1.9251    | 1.8412    | 1.6845    | 1.6285    | 1.5592    | 1.4371    | 1.4177    | 1.1854    | 1.1285    |

| 50  | 1 9961   | 1 9916   | 1 9817   | 1 9601  | 1 9144   | 1 8227   | 1 6570   | 1 6291   | 1 5626   | 1 4273   | 1 4046   | 1 2052   | 1 0997   |
|---|--|--|--|---|--|--|--|--|--|--|--|--|--|
|   | 1.9953   | 1.9900   | 1.9784   | 1.9538  | 1.9028   | 1.8033   | 1.6297   | 1.6290   | 1.5657   | 1.4362   | 1.3726   | 1.2237   | 1.0723   |
| 51  | 1.9944   | 1.9881   | 1.9747   | 1.9469  | 1.8904   | 1.7830   | 1.6303   | 1.6007   | 1.5687   | 1.4447   | 1.3414   | 1.2412   | 1.0460   |
| 52  | 1.9932   | 1.9859   | 1.9706   | 1.9392  | 1.8770   | 1.7618   | 1.6308   | 1.5723   | 1.5715   | 1.4526   | 1.3109   | 1.2577   | 1.0210   |
| 53  | 1.9920   | 1.9835   | 1.9661   | 1.9309  | 1.8628   | 1.7399   | 1.6314   | 1.5742   | 1.5437   | 1.4600   | 1.2812   | 1.2732   | 1.0119   |
| 54  | 1.9905   | 1.9807   | 1.9610   | 1.9219  | 1.8477   | 1.7173   | 1.6318   | 1.5767   | 1.5152   | 1.4670   | 1.2878   | 1.2524   | 1.0360   |
| 55  | 1.9889   | 1.9777   | 1.9554   | 1.9121  | 1.8318   | 1.6942   | 1.6323   | 1.5791   | 1.4868   | 1.4737   | 1.3015   | 1.2245   | 1.0588   |
| 56  | 1.9870   | 1.9742   | 1.9493   | 1.9017  | 1.8151   | 1.6706   | 1.6328   | 1.5814   | 1.4799   | 1.4587   | 1.3146   | 1.1974   | 1.0806   |
| 57  | 1.9849   | 1.9705   | 1.9426   | 1.8905  | 1.7977   | 1.6466   | 1.6332   | 1.5835   | 1.4858   | 1.4308   | 1.3269   | 1.1713   | 1.1013   |
| 58  | 1.9825   | 1.9663   | 1.9354   | 1.8786  | 1.7797   | 1.6336   | 1.6223   | 1.5856   | 1.4914   | 1.4033   | 1.3385   | 1.1460   | 1.1210   |
| 59  | 1.9799   | 1.9617   | 1.9276   | 1.8660  | 1.7610   | 1.6340   | 1.5978   | 1.5875   | 1.4967   | 1.3763   | 1.3495   | 1.1397   | 1.1217   |
| 60  | 1.9770   | 1.9567   | 1.9193   | 1.8527  | 1.7417   | 1.6343   | 1.5894   | 1.5732   | 1.5017   | 1.3600   | 1.3497   | 1.1575   | 1.0983   |
| 61  | 1.9738   | 1.9512   | 1.9103   | 1.8388  | 1.7219   | 1.6347   | 1.5911   | 1.5484   | 1.5065   | 1.3699   | 1.3237   | 1.1745   | 1.0757   |
| 62  | 1.9703   | 1.9453   | 1.9007   | 1.8243  | 1.7016   | 1.6350   | 1.5928   | 1.5237   | 1.5110   | 1.3793   | 1.2983   | 1.1906   | 1.0539   |
| 63  | 1.9665   | 1.9390   | 1.8906   | 1.8091  | 1.6809   | 1.6354   | 1.5944   | 1.5153   | 1.4991   | 1.3882   | 1.2734   | 1.2060   | 1.0330   |
| 64  | 1.9623   | 1.9321   | 1.8799   | 1.7933  | 1.6599   | 1.6357   | 1.5959   | 1.5195   | 1.4746   | 1.3967   | 1.2491   | 1.2207   | 1.0129   |
| 65  | 1.9577   | 1.9248   | 1.8686   | 1.7771  | 1.6387   | 1.6360   | 1.5974   | 1.5234   | 1.4503   | 1.4047   | 1.2347   | 1.2255   | 1.0158   |
| 66  | 1.9528   | 1.9170   | 1.8568   | 1.7603  | 1.6363   | 1.6172   | 1.5988   | 1.5271   | 1.4262   | 1.4124   | 1.2480   | 1.2025   | 1.0355   |
| 67  | 1.9475   | 1.9087   | 1.8444   | 1.7430  | 1.6365   | 1.6001   | 1.5956   | 1.5306   | 1.4197   | 1.4025   | 1.2607   | 1.1802   | 1.0544   |
| 68  | 1.9419   | 1.9000   | 1.8314   | 1.7254  | 1.6368   | 1.6014   | 1.5738   | 1.5340   | 1.4267   | 1.3790   | 1.2728   | 1.1585   | 1.0726   |
| 69  | 1.9358   | 1.8907   | 1.8180   | 1.7074  | 1.6371   | 1.6026   | 1.5520   | 1.5373   | 1.4334   | 1.3559   | 1.2844   | 1.1374   | 1.0900   |
| 70  | 1.9293   | 1.8809   | 1.8041   | 1.6890  | 1.6373   | 1.6038   | 1.5404   | 1.5302   | 1.4397   | 1.3332   | 1.2955   | 1.1170   | 1.1067   |
| 71  | 1.9224   | 1.8707   | 1.7897   | 1.6704  | 1.6375   | 1.6049   | 1.5433   | 1.5085   | 1.4458   | 1.3109   | 1.3061   | 1.1228   | 1.0972   |
| 72  | 1.9151   | 1.8600   | 1.7749   | 1.6515  | 1.6378   | 1.6060   | 1.5462   | 1.4868   | 1.4516   | 1.3162   | 1.2891   | 1.1382   | 1.0780   |
| 73  | 1.9074   | 1.8489   | 1.7597   | 1.6380  | 1.6324   | 1.6070   | 1.5489   | 1.4653   | 1.4572   | 1.3259   | 1.2677   | 1.1530   | 1.0595   |
| 74  | 1.8993   | 1.8373   | 1.7442   | 1.6382  | 1.6132   | 1.6081   | 1.5515   | 1.4625   | 1.4439   | 1.3351   | 1.2467   | 1.16/2   | 1.0415   |
| /5  | 1.8908   | 1.8252   | 1.7282   | 1.6384  | 1.6090   | 1.5938   | 1.5540   | 1.46/6   | 1.4227   | 1.3440   | 1.2263   | 1.1809   | 1.0242   |
|   | $f_{L-1}$  | $f_{L-2}$  | $f_{L-3}$  | $f_{L-4}$   | $f_{L-5}$  | $f_{L-6}$  | $f_{L-7}$  | $f_{L-8}$  | $f_{L-9}$  | $f_{L-10}$   | $f_{L-11}$   | $f_{L-12}$   | $f_{L-13}$   |
| 3   | 0.1842   | 0.0004   | 0.0000   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 4   | 0.6124   | 0.0006   | 0.0000   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 2   | 0.89/0   | 0.0006   | 0.0006   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 0   | 0.9305   | 0.0039   | 0.0006   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| /   | 0.8151   | 0.0159   | 0.0005   | 0.0001  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 0   | 0.7525   | 0.0404   | 0.0003   | 0.0005  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 10  | 0.0078   | 0.1055   | 0.0011   | 0.0005  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 11  | 0.5208   | 0.1707   | 0.0032   | 0.0005  | 0.0001   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 12  | 0.5622   | 0.3123   | 0.0002   | 0.0006  | 0.0002   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 13  | 0.5552   | 0.5303   | 0.0349   | 0.0014  | 0.0005   | 0.0001   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 14  | 0.6858   | 0.5125   | 0.0610   | 0.0030  | 0.0000   | 0.0001   | 0.0000   |  |  |  |  | ()()()()()   | 0 0000   |
| 15  | 0.7929   | 0.0120   |  | <b><i><i>x</i></i></b> <i>ixxxixxxxxxxxxxxxx</i>  | 0.0006   | 0.0002   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |
| 16  | 0.0072   | 0.4983   | 0.0979   | 0.0050  | 0.0006   | 0.0002   | $0.0000 \\ 0.0000$   | 0.0000   | 0.0000   | 0.0000   | 0.0000 0.0000  | 0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000   |
| 17  | 0.88/3   | 0.4983<br>0.4867   | 0.0979<br>0.1460   | 0.0050<br>0.0060<br>0.0111  | 0.0006<br>0.0006<br>0.0008   | 0.0002<br>0.0004<br>0.0006   | $0.0000 \\ 0.0000 \\ 0.0001$   | 0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000   |
| 1/  | 0.8873   | 0.4983<br>0.4867<br>0.4770   | 0.0979<br>0.1460<br>0.2045   | 0.0050<br>0.0060<br>0.0111<br>0.0189  | $\begin{array}{c} 0.0006\\ 0.0006\\ 0.0008\\ 0.0016\end{array}$  | 0.0002<br>0.0004<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0001<br>0.0001   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| 18  | 0.8873<br>0.9694<br>0.9689   | 0.4983<br>0.4867<br>0.4770<br>0.4686   | 0.0979<br>0.1460<br>0.2045<br>0.2716   | 0.0050<br>0.0060<br>0.0111<br>0.0189<br>0.0305  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0003   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\end{array}$  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| 18<br>19  | 0.8873<br>0.9694<br>0.9689<br>0.9100   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446   | $\begin{array}{c} 0.0050\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\end{array}$   | $\begin{array}{c} 0.0006\\ 0.0006\\ 0.0008\\ 0.0016\\ 0.0029\\ 0.0050\\ \end{array}$   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ 0.0003\\ 0.0005 \end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| 18<br>19<br>20  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208   | $\begin{array}{c} 0.0050\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ \end{array}$   | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0050   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0001\\ 0.0001\\ 0.0003\\ 0.0005\\ 0.0006 \end{array}$  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
|   | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148   | $\begin{array}{c} 0.4983 \\ 0.4867 \\ 0.4770 \\ 0.4686 \\ 0.4615 \\ 0.4552 \\ \hline 0.4979 \end{array}$   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498   | $\begin{array}{c} 0.0050\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ \end{array}$  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017   | 0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22     \end{array} $   | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450   | $\begin{array}{c} 0.0030\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.1270\\ \end{array}$   | $\begin{array}{c} 0.0006\\ 0.0006\\ 0.0008\\ 0.0016\\ 0.0029\\ 0.0050\\ 0.0082\\ 0.0129\\ 0.0129\\ 0.0195 \end{array}$   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028   | 0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\     \end{array} $  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427   | $\begin{array}{c} 0.4983\\ 0.4867\\ 0.4770\\ 0.4686\\ 0.4615\\ 0.4552\\ \hline 0.4979\\ 0.5736\\ 0.6466\\ \end{array}$   | $\begin{array}{c} 0.0979\\ 0.1460\\ 0.2045\\ 0.2716\\ 0.3446\\ 0.4208\\ 0.4498\\ 0.4450\\ 0.4408\\ \end{array}$  | $\begin{array}{c} 0.0050\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.1270\\ 0.1649 \end{array}$  | $\begin{array}{c} 0.0006\\ 0.0006\\ 0.0008\\ 0.0016\\ 0.0029\\ 0.0050\\ 0.0082\\ \hline 0.0129\\ 0.0129\\ 0.0195\\ 0.0283 \end{array}$   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044   | 0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$  | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$  | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\     \end{array} $  | $\begin{array}{c} 0.8873\\ 0.9694\\ 0.9689\\ 0.9100\\ 0.8590\\ 0.8148\\ 0.7763\\ 0.7427\\ 0.7158\\ \end{array}$  | $\begin{array}{c} 0.4983\\ 0.4867\\ 0.4770\\ 0.4686\\ 0.4615\\ 0.4552\\ 0.4979\\ 0.5736\\ 0.6466\\ 0.7132\\ \end{array}$   | $\begin{array}{c} 0.0979\\ 0.1460\\ 0.2045\\ 0.2716\\ 0.3446\\ 0.4208\\ 0.4498\\ 0.4450\\ 0.4408\\ 0.4370\\ \end{array}$   | $\begin{array}{c} 0.0050\\ 0.0060\\ 0.0111\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.1270\\ 0.1649\\ 0.2078\\ \end{array}$   | $\begin{array}{c} 0.0006\\ 0.0006\\ 0.0008\\ 0.0016\\ 0.0029\\ 0.0050\\ 0.0082\\ 0.0129\\ 0.0129\\ 0.0195\\ 0.0283\\ 0.0398 \end{array}$   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | $\begin{array}{c} 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ 0.0000\\ \end{array}$   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       \hline       25 \\       \hline       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       \hline       10 \\       10$ | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6872   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4408<br>0.4370<br>0.4337   | 0.0050<br>0.0060<br>0.0111<br>0.0189<br>0.0305<br>0.0466<br>0.0678<br>0.0945<br>0.1270<br>0.1649<br>0.2078<br>0.2255  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0283<br>0.03542<br>0.05942   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       26 \\$             | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6872<br>0.6642   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4408<br>0.4370<br>0.4337<br>0.4307   | 0.0060<br>0.0111<br>0.0189<br>0.0305<br>0.0466<br>0.0678<br>0.0945<br>0.1270<br>0.1649<br>0.2078<br>0.2550<br>0.3055  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       26 \\       27 \\       27 \\       26 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       26 \\       27 \\       26 \\       26 \\       26 \\       27 \\       26 \\       26 \\       26 \\       27 \\       26 \\       27 \\       26 \\$             | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6872<br>0.6642<br>0.6437   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.4208<br>0.44208<br>0.44208<br>0.44208<br>0.4408<br>0.4408<br>0.4370<br>0.4337<br>0.4307<br>0.4280  | 0.0060<br>0.0111<br>0.0189<br>0.0305<br>0.0466<br>0.0945<br>0.1270<br>0.1649<br>0.2078<br>0.2550<br>0.3585<br>0.3585  | 0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0100<br>0.0143<br>0.0199   | 0.0000<br>0.0000<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0027   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       26 \\       27 \\       28 \\       20 \\$             | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479   | $\begin{array}{c} 0.4983\\ 0.4867\\ 0.4770\\ 0.4686\\ 0.4615\\ 0.4552\\ 0.4979\\ 0.5736\\ 0.6466\\ 0.7132\\ 0.6872\\ 0.6642\\ 0.6642\\ 0.6437\\ 0.6255\\ 0.0025\end{array}$  | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.4208<br>0.44208<br>0.4450<br>0.4450<br>0.44370<br>0.4370<br>0.4337<br>0.4307<br>0.4286<br>0.4280   | 0.0060<br>0.0111<br>0.0189<br>0.0305<br>0.0466<br>0.0678<br>0.0945<br>0.1270<br>0.1649<br>0.2078<br>0.2078<br>0.3055<br>0.3055<br>0.3155<br>0.4123  | 0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0977<br>0.1446   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0143<br>0.0199<br>0.0270   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0059   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0013<br>0.0013   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22 \\       23 \\       24 \\       25 \\       26 \\       27 \\       28 \\       29 \\       20 \\$             | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6437<br>0.6255<br>0.6091   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4498<br>0.4450<br>0.4370<br>0.4370<br>0.4307<br>0.4280<br>0.4256<br>0.4628   | $\begin{array}{c} 0.0060\\ 0.0011\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0945\\ 0.0945\\ 0.1270\\ 0.1649\\ 0.2078\\ 0.2550\\ 0.3055\\ 0.3055\\ 0.3135\\ 0.4234\\ 0.4214\\ 0.4214\\ \end{array}$   | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358   | 0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0013<br>0.0013   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0004<br>0.0004   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $ \begin{array}{r} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ \hline 21 \\ \hline \end{array} $  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948<br>0.9722   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6437<br>0.6255<br>0.6091<br>0.5944   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.44208<br>0.4450<br>0.4408<br>0.4450<br>0.4370<br>0.4337<br>0.4307<br>0.4280<br>0.4256<br>0.42680<br>0.5228   | $\begin{array}{c} 0.0060\\ 0.0011\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.2078\\ 0.2550\\ 0.3055\\ 0.3055\\ 0.3585\\ 0.4130\\ 0.4214\\ 0.4105\end{array}$  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0129<br>0.0195<br>0.0283<br>0.0283<br>0.0542<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.2000   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358<br>0.0466   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0029<br>0.0059<br>0.0012   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0003<br>0.0013<br>0.0019<br>0.0022   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0004<br>0.0004   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.000000<br>0.000000<br>0.0000000<br>0.00000000  | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $ \begin{array}{r} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 32 \\ 31 \\ 32 \\ 31 \\ 32 \\ 32 \\ 31 \\ 32 \\ 33 \\ 32 \\ 33 \\ 33 \\ 33 \\ 33 \\ 33$  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948<br>0.9722<br>0.9347   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6437<br>0.6255<br>0.6091<br>0.5944<br>0.5942   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4408<br>0.4450<br>0.4408<br>0.4370<br>0.4337<br>0.4307<br>0.4280<br>0.4280<br>0.4256<br>0.4280<br>0.5228   | $\begin{array}{c} 0.0060\\ 0.0011\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.3055\\ 0.3555\\ 0.3555\\ 0.4130\\ 0.4234\\ 0.4214\\ 0.4195\\ 0.4178\\ \end{array}$   | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0129<br>0.0283<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.1758<br>0.2096<br>0.2460   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0270<br>0.0358<br>0.0466<br>0.0594<br>0.0744   | 0.0000<br>0.0001<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082<br>0.0113<br>0.0152<br>0.0221   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0013<br>0.0019<br>0.0027<br>0.0032   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0001<br>0.0001<br>0.0001   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0001<br>0.0002<br>0.0003<br>0.0004<br>0.0006<br>0.0006   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.00000<br>0.000000<br>0.00000<br>0.00000<br>0.00000000   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000   |
| $ \begin{array}{r} 18\\ 19\\ 20\\ 21\\ 22\\ 23\\ 24\\ 25\\ 26\\ 27\\ 28\\ 29\\ 30\\ 31\\ 32\\ 32\\ 32 \end{array} $   | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948<br>0.9722<br>0.9347<br>0.9005<br>0.8600   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6642<br>0.66437<br>0.6255<br>0.6091<br>0.5944<br>0.5812<br>0.6293<br>0.6801  | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4498<br>0.4450<br>0.4430<br>0.4370<br>0.4337<br>0.4307<br>0.4280<br>0.4256<br>0.4280<br>0.5228<br>0.5767<br>0.5582   | $\begin{array}{c} 0.0060\\ 0.0011\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.0945\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.0555\\ 0.3555\\ 0.3555\\ 0.4130\\ 0.4234\\ 0.4214\\ 0.419\\ 0.4161\\ $ | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.1758<br>0.2096<br>0.245  | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358<br>0.0466<br>0.0594<br>0.0744<br>0.0916   | 0.0000<br>0.0000<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082<br>0.0113<br>0.0152<br>0.0201   | 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| $ \begin{array}{r} 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 26 \\ 27 \\ 28 \\ 29 \\ 30 \\ 31 \\ 32 \\ 33 \\ 34 \\ \end{array} $  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948<br>0.9722<br>0.9347<br>0.9005<br>0.8690<br>0.8403   | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6437<br>0.6255<br>0.6091<br>0.5944<br>0.5812<br>0.6293<br>0.6801<br>0.7288   | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4450<br>0.4450<br>0.4437<br>0.4377<br>0.4307<br>0.4337<br>0.4307<br>0.4280<br>0.4256<br>0.5228<br>0.5583<br>0.5483   | $\begin{array}{c} 0.0060\\ 0.0011\\ 0.0189\\ 0.0305\\ 0.0466\\ 0.0678\\ 0.0945\\ 0.0945\\ 0.1270\\ 0.1270\\ 0.1270\\ 0.0555\\ 0.3555\\ 0.3555\\ 0.3555\\ 0.4130\\ 0.4234\\ 0.4214\\ 0.4195\\ 0.4178\\ 0.4163\\ 0.4148\end{array}$   | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.1758<br>0.2096<br>0.2460<br>0.2485<br>0.3248   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358<br>0.0466<br>0.0594<br>0.0744<br>0.0916<br>0.0111   | 0.0000<br>0.0000<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082<br>0.0041<br>0.0059<br>0.0082<br>0.0113<br>0.0152<br>0.0201<br>0.0201   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0013<br>0.0013<br>0.0027<br>0.0038<br>0.0033<br>0.0071<br>0.0003   | 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0.4178\\ 0.4135\end{array}$  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.1758<br>0.2096<br>0.2460<br>0.2845<br>0.3248<br>0.3663   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358<br>0.0466<br>0.0594<br>0.0744<br>0.0916<br>0.1111<br>0.1329   | 0.0000<br>0.0000<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082<br>0.0041<br>0.0059<br>0.0082<br>0.0113<br>0.0152<br>0.0201<br>0.0201<br>0.0201<br>0.0201   | 0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0001<br>0.0001<br>0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0008<br>0.0013<br>0.0019<br>0.0027<br>0.0038<br>0.0027<br>0.0038<br>0.0071<br>0.0051<br>0.0095<br>0.0124   | 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0.3055\\ 0.3555\\ 0.4130\\ 0.4234\\ 0.4214\\ 0.4195\\ 0.4178\\ 0.4135\\ 0.4135\\ 0.4123\\ \end{array}$  | 0.0006<br>0.0006<br>0.0008<br>0.0016<br>0.0029<br>0.0050<br>0.0082<br>0.0129<br>0.0195<br>0.0283<br>0.0398<br>0.0542<br>0.0718<br>0.0927<br>0.1171<br>0.1449<br>0.2096<br>0.2460<br>0.2845<br>0.3248<br>0.3663<br>0.4086   | 0.0002<br>0.0004<br>0.0006<br>0.0006<br>0.0006<br>0.0010<br>0.0017<br>0.0028<br>0.0044<br>0.0067<br>0.0100<br>0.0143<br>0.0199<br>0.0270<br>0.0358<br>0.0466<br>0.0594<br>0.0594<br>0.0744<br>0.0916<br>0.1111<br>0.1329<br>0.1569                     | 0.0000<br>0.0000<br>0.0001<br>0.0003<br>0.0005<br>0.0006<br>0.0006<br>0.0006<br>0.0006<br>0.0007<br>0.0011<br>0.0018<br>0.0027<br>0.0041<br>0.0059<br>0.0082<br>0.0113<br>0.0152<br>0.0201<br>0.0261<br>0.0333<br>0.0418<br>0.0517   | 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| 17<br>18<br>19<br>20<br>21<br>22<br>23<br>24<br>25<br>26<br>27<br>28<br>29<br>30<br>31<br>32<br>33<br>34<br>35<br>36<br>37<br>38<br>39  | 0.8873<br>0.9694<br>0.9689<br>0.9100<br>0.8590<br>0.8148<br>0.7763<br>0.7427<br>0.7158<br>0.7807<br>0.8410<br>0.8967<br>0.9479<br>0.9948<br>0.9722<br>0.9347<br>0.9005<br>0.8690<br>0.8403<br>0.8138<br>0.8196<br>0.8614<br>0.9009<br>0.9381 | 0.4983<br>0.4867<br>0.4770<br>0.4686<br>0.4615<br>0.4552<br>0.4979<br>0.5736<br>0.6466<br>0.7132<br>0.6642<br>0.6642<br>0.6642<br>0.6642<br>0.6642<br>0.6255<br>0.6091<br>0.5944<br>0.5812<br>0.6293<br>0.6801<br>0.7288<br>0.7754<br>0.7895<br>0.7672<br>0.7466<br>0.7276 | 0.0979<br>0.1460<br>0.2045<br>0.2716<br>0.3446<br>0.4208<br>0.4498<br>0.4450<br>0.4450<br>0.4450<br>0.4370<br>0.4337<br>0.4307<br>0.4307<br>0.4280<br>0.4256<br>0.4680<br>0.5228<br>0.5767<br>0.5692<br>0.5583<br>0.5483<br>0.5392<br>0.5309<br>0.5233<br>0.5163<br>0.5366 | 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|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|-----------|---------|
| 41 | 1.0028 | 0.6937 | 0.6196 | 0.4983 | 0.4073 | 0.3038 | 0.1250 | 0.0466 | 0.0166 | 0.0058 | 0.0020 | 0.0007  | 0.0006    |         |
| 42 | 0.9736 | 0.6786 | 0.6597 | 0.4931 | 0.4065 | 0.3372 | 0.1445 | 0.0557 | 0.0204 | 0.0073 | 0.0026 | 0.0009  | 0.0006    |         |
| 43 | 0.9462 | 0.6985 | 0.6646 | 0.4883 | 0.4057 | 0.3713 | 0.1654 | 0.0661 | 0.0250 | 0.0092 | 0.0034 | 0.0012  | 0.0006    | 1 Fer D |
| 44 | 0.9205 | 0.7361 | 0.6516 | 0.4838 | 0.4059 | 0.4050 | 0.1878 | 0.0776 | 0.0302 | 0.0114 | 0.0043 | 0.0016  | 0.0006    | 1.6     |
| 45 | 0.8963 | 0.7724 | 0.6395 | 0.4797 | 0.4409 | 0.4043 | 0.2116 | 0.0903 | 0.0361 | 0.0140 | 0.0054 | 0.0021  | 0.0008    | *       |
| 46 | 0.8737 | 0.8071 | 0.6282 | 0.4759 | 0.4758 | 0.4038 | 0.2365 | 0.1042 | 0.0429 | 0.0170 | 0.0067 | 0.0026  | 0.0010    | 75      |
| 47 | 0.8524 | 0.8406 | 0.6177 | 0.5107 | 0.4722 | 0.4032 | 0.2625 | 0.1193 | 0.0504 | 0.0206 | 0.0082 | 0.0033  | 0.0013    | 4       |
| 48 | 0.8725 | 0.8323 | 0.6078 | 0.5453 | 0.4688 | 0.4026 | 0.2895 | 0.1357 | 0.0589 | 0.0246 | 0.0101 | 0.0041  | 0.0017    | OF      |
| 49 | 0.9031 | 0.8135 | 0.5985 | 0.5796 | 0.4656 | 0.4020 | 0.3173 | 0.1532 | 0.0683 | 0.0291 | 0.0122 | 0.0050  | 0.0021    |         |
| 50 | 0.9323 | 0.7957 | 0.6132 | 0.5899 | 0.4626 | 0.4015 | 0.3457 | 0.1718 | 0.0786 | 0.0343 | 0.0146 | 0.0062  | 0.0026    |         |
| 51 | 0.9601 | 0.7790 | 0.6463 | 0.5817 | 0.4597 | 0.4010 | 0.3746 | 0.1914 | 0.0898 | 0.0401 | 0.0174 | 0.0075  | 0.0032    |         |
| 52 | 0.9867 | 0.7633 | 0.6786 | 0.5740 | 0.4570 | 0.4039 | 0.4006 | 0.2121 | 0.1020 | 0.0465 | 0.0206 | 0.0090  | 0.0039    |         |
| 53 | 0.9972 | 0.7485 | 0.7100 | 0.5668 | 0.4545 | 0.4334 | 0.4001 | 0.2337 | 0.1151 | 0.0537 | 0.0243 | 0.0108  | 0.0048    |         |
| 54 | 0.9745 | 0.7406 | 0.7344 | 0.5600 | 0.4631 | 0.4521 | 0.3997 | 0.2560 | 0.1292 | 0.0615 | 0.0283 | 0.0128  | 0.0058    |         |
| 55 | 0.9529 | 0.7703 | 0.7212 | 0.5536 | 0.4927 | 0.4498 | 0.3993 | 0.2792 | 0.1442 | 0.0701 | 0.0329 | 0.0152  | 0.0069    |         |
| 56 | 0.9323 | 0.7991 | 0.7087 | 0.5475 | 0.5221 | 0.4477 | 0.3989 | 0.3029 | 0.1600 | 0.0794 | 0.0380 | 0.0178  | 0.0082    |         |
| 57 | 0.9128 | 0.8269 | 0.6969 | 0.5514 | 0.5418 | 0.4457 | 0.3986 | 0.3272 | 0.1767 | 0.0895 | 0.0435 | 0.0207  | 0.0097    |         |
| 58 | 0.8941 | 0.8538 | 0.6857 | 0.5803 | 0.5363 | 0.4437 | 0.3982 | 0.3520 | 0.1943 | 0.1003 | 0.0497 | 0.0240  | 0.0115    |         |
| 59 | 0.8797 | 0.8763 | 0.6750 | 0.6089 | 0.5312 | 0.4419 | 0.3979 | 0.3771 | 0.2125 | 0.1119 | 0.0564 | 0.0277  | 0.0134    |         |
| 60 | 0.9046 | 0.8594 | 0.6650 | 0.6370 | 0.5263 | 0.4401 | 0.4025 | 0.3976 | 0.2315 | 0.1242 | 0.0637 | 0.0318  | 0.0156    |         |
| 61 | 0.9286 | 0.8433 | 0.6646 | 0.6554 | 0.5217 | 0.4385 | 0.4281 | 0.3973 | 0.2512 | 0.1373 | 0.0716 | 0.0362  | 0.0181    |         |
| 62 | 0.9518 | 0.8279 | 0.6916 | 0.6463 | 0.5173 | 0.4537 | 0.4369 | 0.3970 | 0.2714 | 0.1511 | 0.0801 | 0.0412  | 0.0208    |         |
| 63 | 0.9740 | 0.8133 | 0.7180 | 0.6377 | 0.5131 | 0.4794 | 0.4354 | 0.3967 | 0.2921 | 0.1656 | 0.0892 | 0.0465  | 0.0238    |         |
| 64 | 0.9953 | 0.7993 | 0.7438 | 0.6295 | 0.5091 | 0.5050 | 0.4339 | 0.3964 | 0.3133 | 0.1807 | 0.0989 | 0.0524  | 0.0272    |         |
| 65 | 0.9936 | 0.7860 | 0.7690 | 0.6217 | 0.5305 | 0.5053 | 0.4326 | 0.3962 | 0.3349 | 0.1965 | 0.1093 | 0.0587  | 0.0308    |         |
| 66 | 0.9751 | 0.7935 | 0.7732 | 0.6143 | 0.5558 | 0.5017 | 0.4313 | 0.3959 | 0.3568 | 0.2129 | 0.1203 | 0.0655  | 0.0349    |         |
| 67 | 0.9572 | 0.8173 | 0.7611 | 0.6072 | 0.5809 | 0.4983 | 0.4300 | 0.3957 | 0.3790 | 0.2298 | 0.1319 | 0.0728  | 0.0392    |         |
| 68 | 0.9401 | 0.8404 | 0.7495 | 0.6057 | 0.6004 | 0.4950 | 0.4288 | 0.4014 | 0.3955 | 0.2473 | 0.1440 | 0.0806  | 0.0440    |         |
| 69 | 0.9236 | 0.8628 | 0.7384 | 0.6301 | 0.5940 | 0.4918 | 0.4276 | 0.4240 | 0.3953 | 0.2653 | 0.1568 | 0.0890  | 0.0492    |         |
| 70 | 0.9078 | 0.8846 | 0.7278 | 0.6542 | 0.5878 | 0.4888 | 0.4466 | 0.4265 | 0.3950 | 0.2837 | 0.1701 | 0.0978  | 0.0547    |         |
| 71 | 0.9057 | 0.8926 | 0.7176 | 0.6779 | 0.5819 | 0.4860 | 0.4693 | 0.4255 | 0.3948 | 0.3025 | 0.1839 | 0.1072  | 0.0607    |         |
| 72 | 0.9261 | 0.8780 | 0.7079 | 0.7011 | 0.5763 | 0.4919 | 0.4832 | 0.4245 | 0.3946 | 0.3216 | 0.1983 | 0.1171  | 0.0671    |         |
| 73 | 0.9458 | 0.8640 | 0.7239 | 0.6986 | 0.5709 | 0.5145 | 0.4806 | 0.4235 | 0.3945 | 0.3410 | 0.2132 | 0.1275  | 0.0739    |         |
| 74 | 0.9650 | 0.8505 | 0.7462 | 0.6897 | 0.5657 | 0.5369 | 0.4780 | 0.4226 | 0.3943 | 0.3607 | 0.2285 | 0.1384  | 0.0811    |         |
| 75 | 0.9834 | 0.8376 | 0.7680 | 0.6812 | 0.5608 | 0.5592 | 0.4756 | 0.4216 | 0.3941 | 0.3806 | 0.2442 | 0.1497  | 0.0888    |         |

# Appendix B: Figures of real-space representation of HOMOs and LUMOs for the lowest singlet states of fused azulene-acene calculated using spinrestricted TAO-LDA( $\theta = 7$ mHartree) at isovalue = 0.02 eV/Å<sup>3</sup>

Figure B.1: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=7) with their occupation number 1.1880 and 0.8147



Figure B.2: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=8) with their occupation number 1.2742 and 0.7320



Figure B.3: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=9) with their occupation number 1.3406 and 0.6694



Figure B.4: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=10) with their occupation number 1.3927 and 0.6203



Figure B.5: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=11) with their occupation number 1.4323 and 0.5825



Figure B.6: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=12) with their occupation number 1.4628 and 0.5529



Figure B.7: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=13) with their occupation number 1.4257 and 0.5668



Figure B.8: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=14) with their occupation number 1.3102 and 0.6857



Figure B.9: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=15) with their occupation number 1.2068 and 0.7927

Figure B.10: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=16) with their occupation number 1.1160 and 0.8871



Figure B.11: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=17) with their occupation number 1.0372 and 0.9693



Figure B.12: Real-space representation of HOMO (left) and LUMO (right) for the singlet state of fused azulene-acene (n=18) with their occupation number 1.0405 and 0.9688



Figure B.13: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=19) with their occupation number 1.1018 and 0.9099



Figure B.14: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=20) with their occupation number 1.1547 and 0.8589



Figure B.15: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=21) with their occupation number 1.2006 and 0.8146



Figure B.16: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=22) with their occupation number 1.2405 and 0.7761



Figure B.17: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=23) with their occupation number 1.2752 and 0.7426



Figure B.18: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=24) with their occupation number 1.2782 and 0.7158



Figure B.19: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=25) with their occupation number 1.2165 and 0.7807



Figure B.20: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=26) with their occupation number 1.1593 and 0.8409



Figure B.21: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=27) with their occupation number 1.1063 and 0.8967



Figure B.22: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=28) with their occupation number 1.0577 and 0.9478



Figure B.23: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=29) with their occupation number 1.0131 and 0.9948



Figure B.24: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=30) with their occupation number 1.0379 and 0.9721



Figure B.25: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=31) with their occupation number 1.0772 and 0.9347



Figure B.26: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=32) with their occupation number 1.1131 and 0.9004



Figure B.27: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=33) with their occupation number 1.1461 and 0.8690



Figure B.28: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=34) with their occupation number 1.1762 and 0.8402



Figure B.29: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=35) with their occupation number 1.2038 and 0.8138



Figure B.30: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=36) with their occupation number 1.1789 and 0.8195



Figure B.31: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=37) with their occupation number 1.1394 and 0.8614



Figure B.32: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=38) with their occupation number 1.1021 and 0.9008



Figure B.33: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=39) with their occupation number 1.0669 and 0.9380



Figure B.34: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=40) with their occupation number 1.0339 and 0.9730



Figure B.35: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=41) with their occupation number 1.0059 and 1.0027



Figure B.36: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=42) with their occupation number 1.0367 and 0.9736



Figure B.37: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=43) with their occupation number 1.0657 and 0.9462



Figure B.38: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=44) with their occupation number 1.0928 and 0.9204

(0.9204)

Figure B.39: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=45) with their occupation number 1.1182 and 0.8963



Figure B.40: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=46) with their occupation number 1.1420 and 0.8737





Figure B.42: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=48) with their occupation number 1.1286 and 0.8725



Figure B.43: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=49) with their occupation number 1.0998 and 0.9031

Figure B.44: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=50) with their occupation number 1.0723 and 0.9323

$$(1.0723)$$

Figure B.45: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=51) with their occupation number 1.0460 and 0.9601



(0.9745)

Figure B.49: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=55) with their occupation number 1.0588 and 0.9529

Figure B.50: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=56) with their occupation number 1.0806 and 0.9323

= (1.0806)

<sup>5</sup>(0.9529)

Figure B.51: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=57) with their occupation number 1.1013 and 0.9127

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Figure B.52: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=58) with their occupation number 1.1210 and 0.8941

Figure B.53: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=59) with their occupation number 1.1217 and 0.8797

Figure B.54: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=60) with their occupation number 1.0983 and 0.9046

1,0983)

Figure B.55: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=61) with their occupation number 1.0757 and 0.9286

(1.0757)

Figure B.56: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=62) with their occupation number 1.0540 and 0.9517

Figure B.57: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=63) with their occupation number 1.0331 and 0.9740

Figure B.58: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=64) with their occupation number 1.0130 and 0.9953

• (0.9953)

Figure B.59: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=65) with their occupation number 1.0159 and 0.9936

Figure B.60: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=66) with their occupation number 1.0355 and 0.9750

Figure B.61: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=67) with their occupation number 1.0545 and 0.9572

Figure B.62: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=68) with their occupation number 1.0726 and 0.9401

Figure B.63: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=69) with their occupation number 1.0900 and 0.9236

Figure B.64: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=70) with their occupation number 1.1068 and 0.9078

(0.9078)

Figure B.65: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=71) with their occupation number 1.0972 and 0.9057

Figure B.66: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=72) with their occupation number 1.0781 and 0.9261

(0.9261)

Figure B.67: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=73) with their occupation number 1.0595 and 0.9458

(1.0595)

Figure B.68: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=74) with their occupation number 1.0416 and 0.9649

Figure B.69: Real-space representation of HOMO (up) and LUMO (down) for the singlet state of fused azulene-acene (n=75) with their occupation number 1.0242 and 0.9834